



"APPROVED FOR RELEASE: 06/05/2000

CIA-RDP86-00513R000100510020-2

DEM'YANOV, L.A., kand.tekhn.nauk; AKHTYAMOV, U.S.; AGEYEV, I.V.; PAKHOMOV, K.A.  
SARAFANOV, S.K.

Performance of IaAZ-204 engines fueled with light gasoline. Avt.prom.  
no.2:23-27 F '61. (MIRA 14:3)  
(Automobiles—Engines)(Gasoline)

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CIA-RDP86-00513R000100510020-2"

USSR / General Biology. General Histology.

3

Abs Jour : Ref Zhur - Bioll, No 19, 1953, № 85562

Authors : Bazarnova, N. A.; Aseyev, I. Ya.

Inst : Not Given

Title : Neutrophilic Granulosity in Electron Microscopy  
Picture.

Orig Pub : Labor. dobo, 1957, No. 3, 16..19

Abstract : A study by electron microscopy was conducted on blood of healthy humans and patients ill with cancer of the uterine cervix complicated by peritonitis. The neutrophile granulosity of the patients is polymorphous. Round, oval, rod-shaped, and granules of an indefinite form of a magnitude of 60 x 85 up to 450 x 540  $\mu$ m are encountered. Large and medium size granules are

Card 1/2

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AGEEYEV, I.Ya.

Electron microscope studies on Pasteurella pestis in the blood of infected pigs [with summary in English]. Vop.virus 3 no.4:221-225  
Jl-Ag '58 (MIRA 11:9)

1. Ukrainskiy nauchno-issledovatel'skiy institut experimental'noy veterinarii, Khar'kov.

(PASTEURELLA PESTIC,  
electron microscopy in infect hog blood (Rus))

(MICROSCOPY, ELECTRON,  
of Pasteurella pestis in infected hog blood (Rus))

AGEYEV, I. Ya., Candidate Vet Sci (diss) -- "The immunobiology and electric microscopy of the swine-plague virus". Khar'kov, 1959. 25 pp (Min Agric USSR, Khar'-kov Vet Inst), 200 copies (KL, No 24, 1959, 147)

8 (5)

## AUTHOR:

Ageyev, I. Z., Engineer (Moscow)

SOV/105-59-11-11/32

## TITLE:

The Changes in the Characteristics of Electric Motors With  
High Velocity Range

## PERIODICAL:

Elektrichestvo, 1959, Nr 11, pp 52 - 56 (USSR)

## ABSTRACT:

In the introduction the influence exercised by the armature reaction of the current of commutating sections and of the voltage of the reversing poles on the terminal voltage is discussed and equation (1) for the terminal voltage is written. The last three terms in this formula may reduce or increase the voltage decrease. In the first part the influence exercised by the current in the commutating sections on the main field is dealt with. By figure 1 this influence is explained for accelerated and decelerated commutation, and equation (8) is deduced for the magnetizing force of the commutating sections. In figure 2 the dependence of the magnetizing force on the load for a maximum number of revolutions (9000 rpm) is represented. With low load commutation is accelerated, for loads with more than 100% it is decelerated and it is found that if the effect of the commutating sections agrees with the direction of the armature reaction a deformation of the characteristics and an unsteady

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The Changes in the Characteristics of Electric Motors SOV/105-59-11-11/32  
With High Velocity Range

performance of the motor is observed. This is explained in more detail by the diagrams in the figures 3,4, and 5 for an airplane generator. Furthermore it is said that with increasing load the transverse armature reaction (Poperechnaya reaktsiya yakorya) and the exciter current increase. In compensated generators the effect of the cross armature reaction is eliminated and the influence of the magnetizing factors is increased. In the final part the longitudinal armature reaction and the asymmetry of the field of the reversing poles is dealt with. In this connection a six-pole machine with a power of 6 kw is discussed. The investigations showed that a shift of the brushes and the influence of the commutating sections considerably change the control characteristics for a maximum number of revolutions i.e. in machines with equal and half the number of reversing pole of the field poles. In a symmetrical arrangement of the reversing poles to the neutral line no influence is found to be exercised on the main field since one half of the field of the reversing poles is summed with the

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The Changes in the Characteristics of Electric Motors SOV/105-59-11-11/32  
With High Velocity Range

main field, the other is subtracted. If the reversing poles are shifted in the rotation direction and if the brushes are shifted in opposite direction an EMF is produced in the armature coils for the calculation of which a formula is given. Thus a "decrease" in the control characteristics is brought about. A stable performance of the machines with reversing poles cannot be achieved by shifting the brushes in the opposite direction to the armature; a shift in the rotation direction of the armature shows a positive effect with a slight increase in the minimum spin. To obtain a satisfactory commutation in the shift of the brushes the pole shoes of the reversing poles must be lengthened in the direction of the armature rotation direction. There are 8 figures.

SUBMITTED: February 14, 1959

Card 3/3

AGEYEV, I.Z., inzh. (Moskva)

Distribution of magnetic flux and commutating field in machines  
having a full or half number of supplementary poles. Elektrichest-  
vo no.3:38-43 Mr '60. (MIRA 13:6)  
(Electric machinery)

8619

16.9500 (1031,1132,1222)

S/105/60/000/012/004/006  
B012/B058AUTHOR: Ageyev, I. Z., Engineer (Moscow)

TITLE: Conditions for Commutating Machines With a Wide Speed Range

PERIODICAL: Elektrichestvo, 1960, No. 12, pp. 61-69

TEXT: With a view to the fact that it is very difficult to obtain a good commutation in d.c. machines with a wide speed range ( $n_{\max}/n_{\min} \geq 3$ ), the conditions for such a commutation are studied here. The commutation for machines with and without commutating poles is investigated. The zone of non-sparking commutation, the tuning of commutation according to the oscillograms of field and current in the coil, as well as the influence of brush heating and other factors on commutation are dealt with. The following statements are made on the basis of these explanations: For machines without commutating poles and with wide speed ranges it is suitable to mount the brushes in the neutral plane. For lowest and medium speed of machines with half the number of commutating poles, the zone of dark commutation is much wider than for machines with all commutating

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Conditions for Commutating Machines With a  
Wide Speed Range

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poles. At maximum speeds and the same electromagnetic loads, the zone of dark commutation is less wide for machines with half the number of commutating poles than for those with all commutating poles, and that owing to the change of the field form in the commutation zone without commutating poles. At equal weight and dimensions, the machine with all commutating poles always shows a greater electromagnetic load (by 15-20%) and a greater reactive emf  $e_r$ . The experiments show that for the manufacture of newly designed machines with a wide speed range, the main difficulties arise when tuning commutation for maximum speed, that is, when  $e_r$  and  $e_r - e_k$ , respectively, reach maximum values.  $e_k$  is the commutating emf. In this connection it is pointed out that the M. F. Karasev's statement (Ref. 4) that the function  $e_r = f(n)$  is represented by straight lines parallel to the abscissa is wrong. The dark commutating zone can be absent in heavily utilized controllable machines at maximum speed and the commutating field  $B_k$  has an unfavorable form. For this reason, a displacement of the brushes from the neutral zones by a maximum of 1.0 mm should be permitted apart from the proper selection of the pole-shoe shape of the commutating pole (Ref. 2). The commutation in

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Conditions for Commutating Machines With a  
Wide Speed Range

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newly designed machines should be tuned by varying the main pole air gap and the commutating pole air gaps. Thus, not only the size but also the shape of the commutation field is changed. From the oscillogram it may be seen that the current change during commutation takes place only if commutation is slowed down. When commutation is accelerated, the current change proceeds along a continuous curve. It appears that in this case the commutation time is smaller than the calculated one. If commutation is slowed down, the commutation time equals the calculated value.

Commutation,  $e_r$ , and the field form are largely dependent on the type and construction of the winding. It is recommended to use a winding with  $u_k = 1$  and a shortened slot pitch for facilitating the commutation of heavily utilized machines with a wide speed range and a capacity of more than 18 kw. If possible, a combined frog-leg winding should be used. Experience has shown that machines with half the number of commutating poles show sufficient commutation if the linear load is  $A \leq (350-400)$  a/cm and  $e_r \leq 3.5$  v. There are 11 figures, 1 table, and 5 Soviet references.

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Conditions for Commutating Machines With a  
Wide Speed Range

S/105/60/000/012/004/006  
B012/B058

SUBMITTED: July 29, 1960

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AGEYEV, I.Z., inzh. Moskva)

Effect of the nonsymmetry of the magnetizing force of the main  
poles on the commutating poles and on the operating characteristics  
of machines. Elektrichestvo no.9:37-40 S '61. (MIRA 14:9)  
(Electric machinery)

AGEYEV, I.Z., inzh. (Moskva)

Features of the selection of armature windings of certain d.c.  
machinery. Elektrichesvo no.11:48-55 N '61. (MIRA 14:11)  
(Electric machinery--Windings)

AGEYEV, I.Z. (Moskva)

Short-circuit current in electric generators with a wide range  
of speeds. Elektrichesivo no.1:45-48 Ja '62. (MIRA 14:12)  
(Electric generators)

AGEYEV, I.Z. (Moskva)

Nonstable operation and self-oscillations in the automatic control  
systems of d.c. machines with distorted characteristics,  
Elektrichestvo no.5:56-60 My '64. (MIRA 17:6)

DIBNER, V.D.; AGEYEV, K.S.

Mesozoic deposits on the islands of Severnaya Zemlya. Inform. biul.  
NIIGA no. 15:9-18 '60. (MIRA 14:6)  
(Severnaya Zemlya—Geology, Stratigraphic)

AGFEYEV, K.S.; DITMAR, A.V.

Some characteristics of the relief of high-mountainous  
regions in the Koryak Highland. Uch. zap. NIIGA. Reg.  
geol. no.4:137-150 '64. (MIRA 18:12)

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AGEYEV, L. N., SUKANSKIY, A. V., and KHARIN, S. Ye.

"Colloids of Diffused Sap," Zh. Sakharn. rrom., 5, 591, 1931.

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CIA-RDP86-00513R000100510020-2"

FIGEYEV, L.M.

1ST AND 2ND DEPARTMENTS OF THE NEW YORK STATE BAR ASSOCIATION

**Peptization of pectin substances in diffusion.** *J. Am. Accts. & Proces. Chem.* 1932, 12, 1088. — Peptization of pectin substances in sugar diffusion greatly increases above 80° for ripe beets and above 75° for unripe beets. Duration of heating up to 10 min. is without much effect. At 85° 1.30 times as much pectin substances were diffused into the juice as at 80°. Peptization is at a min. at about pH 5.0; at pH 7.0, it is 2.35 times higher than at 3.0. Antipeptizing agents should be selected capable of decreasing the pH to an optimum and reducing the swelling ability of the pectin substances and coagulating them at the moment of peptization. Doubling the surface of the beet shaving left the extent of peptization unaffected. In a battery, the middle diffusers are responsible for most pectin substances passing into the juice; this is thought to be connected with the effect of temp. A colorimetric method (Sili and Silina, *C. A.*, 28, 874) was found to be applicable to research on the effect of pectin substances on diffusion. *J. G. Tolpin*

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## **METALLURGICAL LITERATURE CLASSIFICATION**

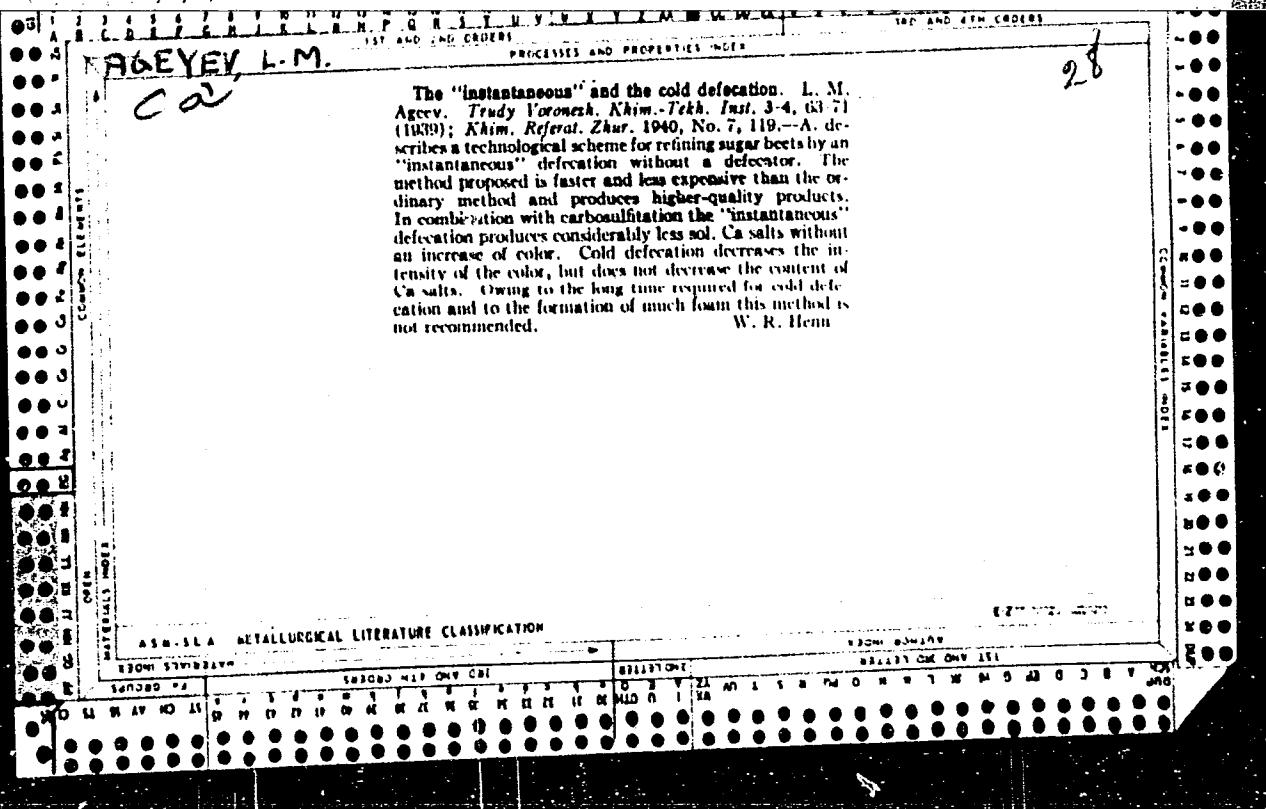
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CIA-RDP86-00513R000100510020-2"



L. M. Agoren'. Candidate of Technical Sciences, and S. A. Korol'kov, Candidate of Technical Sciences, Metodicheskaya kniga po voprosam i posledovatel'nym etapam selenizatsii i sulfato-vinsitovo proizvodstva (Chemico-Technical Control and Calculation of Hydrolytic, and Sulfite Production of Alcohol). Gorles. unisdat.

The booklet gives investigation methods for raw materials, intermediate, and finished products, waste, auxiliary materials used, and includes plans for calculation of hydrolytic, and sulfite production of alcohol, and the production of pravite, celose, furfurol, bonding agents, and vanillin.

The booklet is intended for Forestry Institute students.

SO: Sovetskaya kniga (Soviet Books), No. 116, 1953, Moscow, (U-6472)

AGEYEV, L.M.; KOROL'KOV, S.I.; ZAKOSHCHIKOV, A.P., redaktor; VOL-  
KHOVSKY, R.S., tekhnicheskiy redaktor.

[Chemical and technical control and accounting in hydrolyte and  
sulfite liquor production] Khimiko-tehnicheskii kontrol' i  
uchet gidrolizmogo i sul'fitno-spirtovogo proizvodstva. Moskva,  
Goslesbunizdat, 1953. 403 p. (MIRA 7:8)  
(Wood pulp industry)

AGEYEV, L.M., kand. tekhn. nauk, dotsent; BABIN, F.P., kand. tekhn. nauk, dotsent; SMIRNOV, V.A., doktor tekhn. nauk, prof.; SOFRONOV, G.F., kand. tekhn. nauk, dotsent, red.; IVANOV-RECHNOY, I.Ya., red.; NAUMOV, K.M., tekhn. red.

[Technology of the main branches of industry] Tekhnologija vazhneishikh otraspeli promyshlennosti; uchebnoe posobie dlja vysshikh partii-nykh shkol. Pod red. G.V.Sofronova. Moskva, Izd-vo VPSh i AON pri TsK KPSS. Part 4. [Food industry] Pishchevaja promyshlennost'. 1961. 189 p.

(MIRA 14:6)

(Food industry)

"APPROVED FOR RELEASE: 06/05/2000

CIA-RDP86-00513R000100510020-2

AGEYEV, Leonid Mikhaylovich, dots.; IVANOV, Sergey Zakharovich, prof.;  
SMIRNOV, Valentin Aleksandrovich, prof.; SILIN, P.M., prof.,  
red.; MURASHOVA, O.I., red.; SOKOLOVA, I.A., tekhn. red.

[Technology of sugar substances; general course] Tekhnologija  
sakharistykh veshchestv; obshchii kurs. Pod red. P.M.Silina.  
Moskva, Pishchepromizdat, 1961. 488 p. (MIRA 15:3)  
(Sugar) (Starch)

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CIA-RDP86-00513R000100510020-2"

VYDRIN, V.N.; AMOSOV, P.N.; AGEYEV, L.M.

Dynamometer with a nonamplifying circuit and resistance strain  
gauges. Izm. tekhn. no.8:24-25 Ag '63. (MIRA 16:10)

VYDRIN, V.N.; AGEYEV, I.M.

Effect of expansion in width on the form of the epure of  
contact stresses. Izv. vys. ucheb. zav.; chern. met. &  
no.11:69-73 '65. (VIF A 18:11)

1. Chelyabinskij politekhnicheskiy institut.

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CIA-RDP86-00513R000100510020-2

LIKHACHEV, N.V.; NAZAROV, V.P.; AGEYEV, I.S.; BORISOVICH, Yu.F.; LYUBASHENKO,  
S.Ya.; KORNEYEV, I.P.; MALTSEKHOV, Yu.A.; YURKOV, G.G.

Book reviews and bibliography. Veterinariia 40 no.8:86-89 Ag '63.  
(MIRA 17:10)

APPROVED FOR RELEASE: 06/05/2000

CIA-RDP86-00513R000100510020-2"

AGIRBICEANU, L; HAGIESCU, M.

Temperature of rotation in the CH(\lambda 3889A) band emitted by the Bunsen flame. p. 1263. Academia Republicii Populare Romine. COMUNICARILE. Bucuresti. Vol. 5, no. 6, June 1955.

SOURCE: East European Accessions List (EEAL) Library of Congress, Vol. 5, no. 9, Sept. 1955

AGIRBICEANU, L. AND OTHERS

Effect of argon on the spectrum of vapors of I<sub>2</sub>. p. 1439.  
Academia Republicii Populare Romine. COMUNICARILE. Bucuresti.  
Vol. 5, no. 10, Oct. 1955.

SOURCE: East European Accessions List (EEAL) Library of Congress, Vol. 5,  
no. 9, Sept. 1955

AGEYEV, M. (Rostov-na-Donu); KANUKOV, G. (Rostov-na-Donu)

Center of grain in 35 minutes. Sov. profsoiuzy 18 no.6:8  
Mr '62. (MIRA 15:3)

1. Sekretar' Rostovskogo oblastnogo komiteta profsoyuza rabochikh i sluzhashchikh sel'skogo khozyaystva i zagotovok (for Ageyev).
2. Instruktor Rostovskogo oblastnogo soveta profsoyuzov, neshtatnyy korrespondent zhurnala "Sovetskiye profsoyuzy" (for Kanukov).

(Rostov Province--Grain)

AGEYEV, M.D., (Leningrad)

Approximate theory of magnetic-modulated data transmitters.  
Avtom. i telem. 17 no.8:746-758 Ag '56. (MLRA 9:10)

(Magnetic instruments)

S/196/63/000/002/019/026  
E194/E155

AUTHOR: Ageyev, M.D.

TITLE: Modeling of heat-transfer equipment

PERIODICAL: Referativnyy zhurnal, Elektrotehnika i energetika,  
no.2, 1963, 7, abstract 2 G 33. (Dokl. 4-y Mezhvuz.  
konferentsii po primeneniyu fiz. i matem. modelirova-  
niya v razlichn. otrazlyakh tekhn. Sb.3. (Reports of  
the 4th Intercollegiate Conference on the Application  
of Physical and Mathematical modeling in various  
branches of technology. Collection 3). Moscow, 1962,  
243-251)

TEXT: A method of modeling heat-exchange processes for two  
of the most simple cases is proposed; the temperature of the  
secondary heat-transfer medium is the same throughout the length  
of the coil carrying the primary medium; and the temperature of  
the secondary medium varies in a given direction according to a  
linear law. Special methods of modeling are required, because  
standard electronic models will not directly solve differential  
equations in the partial differential coefficients which describe  
the processes of heat and mass exchange. Models intended for  
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Modeling of heat-transfer equipment

S/196/63/000/002/019/026  
E194/E155

solving boundary problems' cannot be used either. With the above-mentioned assumptions, the methods proposed describe the dynamics of the secondary medium by ordinary differential equations. These assumptions are valid in the solution of numerous problems, for instance, in cases of transverse flow of secondary medium over a coil and that of relatively slow flow of secondary medium in a longitudinal direction. In the methods considered the modeling diagrams differ from those used in systems with concentrated parameters in the presence of an element which introduces delay. The delay process may be modeled by various devices, such as a standard delay unit type 6M-3 (BP-3). It is better to use a device which models the relationship:

$$\lim_{n \rightarrow \infty} \left( \frac{1}{1 + \frac{T}{n} p} \right)^n = e^{-Tp}$$

[Abstractor's note: Complete translation.]

Card 2/2

AGEYEV, M.D. (Vladivostok)

"Optimum structure of an amortization system for random forces"

report presented at the 2nd All-Union Congress on Theoretical and Applied Mechanics, Moscow, 29 January - 5 February 1964

AGEYEV, M.I.; PODDEBYUGIN, V.B., ott. red.; GLOVA, I.A., red.

[Principles of the "Algol-60" algorithmic language.] Osnovy algoritmičeskogo jazyka Algol-60. Moskva, 1964. 114 p. (Akademija nauk SSSR. Vychislitel'nyi tsentr. Obshchie voprosy programirovaniia, no.1).  
(KHA 17:10)

AGEYEV, Mikhail Vasil'yevich; GOLUBNICHIIY, I.S., prof., doktor  
ekon.nauk. red.; PASKIN, I., red.izd-va; MAKEYCHEVA, Ye.,  
red.izd-va; POPOVA, M., tekhn.red.

[Victory of collective farming in Mordovia] Pobeda kolkhoznogo  
stroia v Mordovskoi ASSR. Pod red. I.S.Golubnichego. Saransk,  
Mordovskoe knizhnoe izd-vo, 1960. 413 p.

(MIRA 14:2)

(Mordovia--Collective farms)

DANILOV, Grigoriy Grigor'yevich, kand. sel'khoz. nauk; AGEYEV,  
M.V., doktor ekon. nauk, prof., otv. red.; YEGOROV, V.,  
red.

[From the history of agriculture in Mordovia] Iz istorii  
zemledeliia Mordovii. Saransk, Mordovskoe knizhnoe izd-  
vo, 1964. 110 p. (MIRA 17:8)

SNESAREV, K.A.; VOROB'YEVA, M.T.; AGEYEV, M.Ye.

Rapid method for determining the temperature of colophony  
softening. Gidroliz. i lesokhim. prom. 9 no.4:17-18 '56.  
(MLRA 9:11)

1. TSentral'nyy nauchno-issledovatel'skiy lesokhimicheskiy  
institut.  
(Gums and resins)

AGEYEV, M.Ye.

Magnetic level indicator. Gidroliz. i lesokhim. prom. 10 no.3:  
21-22 '57. (MLRA 10:5)

1. TSentral'nyy nauchno-issledovatel'skiy lesokhimicheskiy  
institut.  
(Liquid level indicators)

AGEYEV, N.

At a complex production. Prof.-tekhn. obr. 18 no.9:9-10 S '61.  
(MIRA 14:11)

1. Direktor tekhnicheskogo uchilishcha No.5, Novosibirsk.  
(Novosibirsk--Vocational education)

1. KOGAN, A. Ya.; GAVRIKOV, V. A.; KHMELEV, A. P.; AGEYEV, N. A.; KULEMENA, Ye. A.
2. USSR (600)
4. Horses
7. Results of raising colts on the collective farms of the Pochinok State Breeding Farm. Konevodstvo 22 no. 12 1952.
9. Monthly List of Russian Accessions, Library of Congress, April 1953, Uncl.

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S/182/60/000/007/005/016  
A162/AC29

AUTHOR: Ageyev, N.P.

TITLE: Investigations of the Temperature-Speed Factor in Plastic Deformation of Metals ✓

PERIODICAL: Kuznechno-shtampovochnoye proizvodstvo, 1960, No. 17, pp. 17 - 21

TEXT: There is no proved theory explaining the effect of the deformation speed on the mechanical properties of deformed metal and there are as yet no special test machines for experiments with hot metal and very fast deformation. This article presents a review of different test machines with brief design and operation descriptions: the rotary machine of A. Nadai and M. Menzhoyn, with mechanical drive for tests of metal properties at  $135$  to  $900 \text{ sec}^{-1}$  and high temperature and a machine of a similar principle (Fig. 1) with heavy flywheel, mounted on a rolling mill stand described in (Ref. 6) in which deformation is recorded by photoelectric or electric means. A rotary machine with force transmission to the specimen through a flexible tie rod (Fig. 2) (Ref. 7); a machine with loading by means of chain transmission (Fig. 3); a machine for tension and compression (Fig. 4), (Ref. 8) under loads up to 1,000 kg at temperatures between

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S/182/60/000/007/005/016  
A162/A029

Investigations of the Temperature-Speed Factor in Plastic Deformation of Metals

-195 to +800°C and 0.03 - 52 mm/sec deformation; a machine with a multi-thread screw (Fig. 5), including a variator of IsNITMASH design, a V-belt transmission electric 1.5 kw motor, and heavy sheaves. A hydraulic test machine for 500 kg maximum load designed at the LVMI with deformation speed controllable within a range of 1 to 100 mm/sec. The electric feed circuit and high frequency amplifier and the bridge for measuring deformation in this latter machine are illustrated by circuit diagrams. This machine has been in use for 6 months and has been found satisfactory. There are ..... 9 references: 7 Soviet, 1 German, 1 British.

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Card 2/6

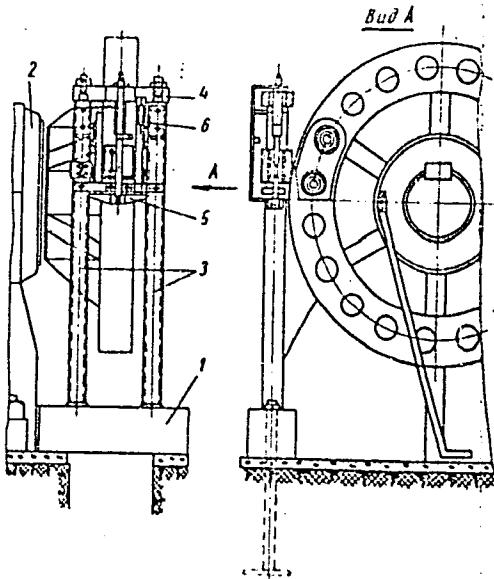
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A162/A029

Investigations of the Temperature-Speed Factor in Plastic Deformation of Metals

Figure 1:

High-Speed Installation Mounted  
on the Base of a Rolling Mill  
Stand 1-support; 2-flywheel bearing;  
3-supporting columns; 4-cross-  
head; 5-anvil rigidly fastened with  
the sample; 6-core of electromagnet.



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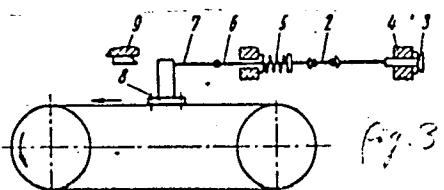
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S/182/60/000/007/005/016  
A162/A029

Investigations of the Temperature-Speed Factor in Plastic Deformation of Metals

Figure 2:

Diagram of an Experimental Drop Hammer for Investigating Metals in the Hot State:  
1-flywheel; 2-pin; 3-flexible tie rod; 4-wedge-shaped support for removing the tie rod clamps  
5-upper clutch; 6-elastic dynamometer; 7-furnace; 8-lower clutch.



Card 4/6

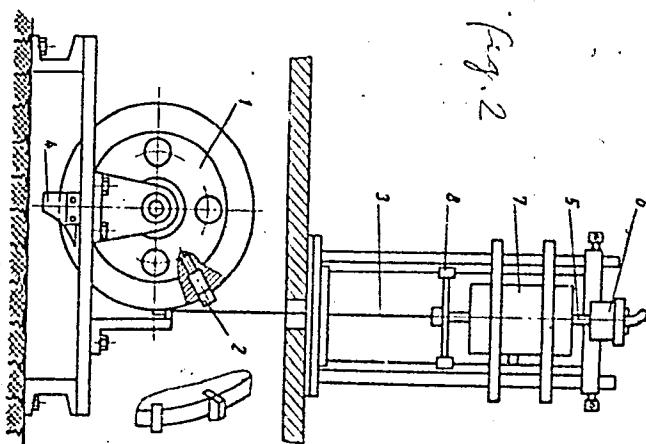


Figure 3: Diagram of the Loading Mechanism of an Experimental Machine With Chain Transmission:  
1-loading chain; 2-sample; 3-elastic element;  
4-support; 5-spring; 6-hinge; 7-tie rod; 8-carriage; 9-wedge

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A162/A029

Investigations of the Temperature-Speed Factor in Plastic Deformation of Metal

Figure 4:

Kinematic Diagram of a Machine  
for Tension and Compression Tests  
at Various Rates and Temperatures:  
1-electromotors; 2-connecting piece;  
3 and 4-worm gears; 5-master form;  
6-elastic element; 7-clutches; 8-  
casing; 9-12-photoelectric instal-  
lation for measuring and recording  
forces and deformations

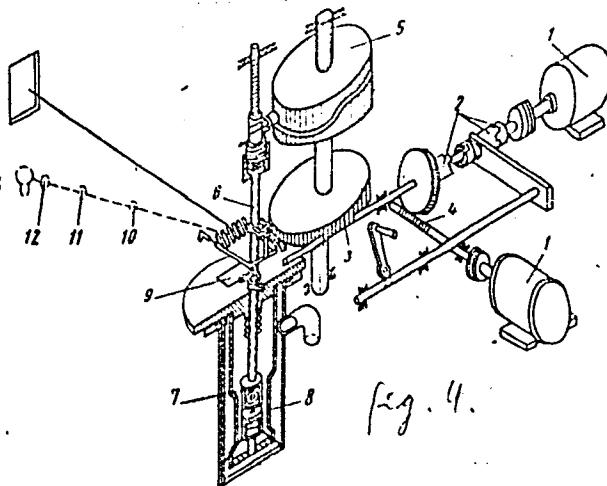


fig. 4.

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Card 5/6

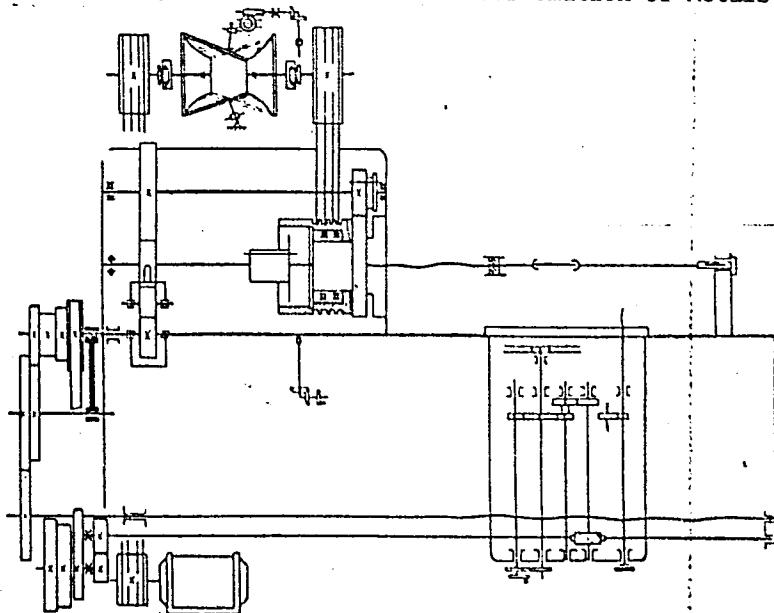
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S/182/60/000/007/005/016  
A162/A029

Investigation of the Temperature-Speed Factor in Plastic Deformation of Metals

Figure 5:

Kinematic Diagram of  
the Loading Mechanism  
of a Machine for Ten-  
sion Tests at Various  
Deformation Rates.



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S/902/62/000/000/003/015  
E195/E583

AUTHOR: Ageyev, N.P.

TITLE: The effect of temperature and strain-rate on the workability of steels

SOURCE: Novyye protsessy obrabotki metallov davleniyem; doklady Soveshch. po novym prots. oprab. met. davleniyem v mashinostr., 1960. Ed. by V. D. Golovlev. Moscow, Izd-vo AN SSSR, 1962. 53 - 60

TEXT: The present investigation, directed by Professor, Doctor of Technical Sciences G.A. Smirnov-Alyayev, was conducted at the metal-working department of the Leningradskiy mekhanicheskiy institut (Leningrad Mechanical Institute). Its object was to determine the effect of temperature and strain-rate (in the  $10^{-5}$  -  $10^1 \text{ sec}^{-1}$  range) on the mechanical properties of steels and other alloys with a view to providing accurate and comprehensive data necessary for studies of various metal-working processes. The tests were carried out on a specially designed tensile-testing

Card 1/3

## The effect of temperature ....

S/902/62/000/000/005/015  
E193/E383

machine equipped with a tensometer and an oscillograph for recording both the loads and strains. The experimental materials included brass D62 (L62) and steels 1X13 (1Kh13), 1X18N9T (1Kh18N9T), 45, Y-7 (U-7). The tensile tests were conducted at 800 - 1200 °C. Analysis of the results obtained led to the following conclusions: 1) The relationship between the true tensile strength  $\sigma'$  and the strain-rate  $v$  is described by  $\sigma' = \sigma'_0 + Klnv$  for the 1Kh18N9T steel and by:

$$\frac{\sigma'}{\sigma'_0} = \left( \frac{v}{v_0} \right)^N \quad (1)$$

for the other materials studied. 2) In the case of alloys with a relatively low melting point, the maximum effect of the strain rate on  $\sigma'$  is shifted towards temperatures approaching the melting point. 3) The strain-rate dependence of the critical values of stable deformation  $M_\epsilon$  can be described by  $M_\epsilon = 1/(a - b \log v)$ . 4) On increasing the strain-rate to  $10^{-1}$  sec<sup>-1</sup> the reduction in area of steel 1Kh13 increases, decreasing at strain rates greater than  $10^{-1}$  sec<sup>-1</sup> (the reduction in area of steels 45 and U-7 in Card 2/3).

The effect of temperature .....

S/902/62/000/000/003/015  
E193/E383

the entire range of temperatures and strain rates studied was 97 - 100%). 5) A clearly defined relationship between the strain rate and plasticity was observed only for steel 1Kh13 at 1100 - 1200 °C; on increasing v from the lowest to the upper limit of the range studied, the plasticity of this steel increased by 70 - 80%. 6) Steels 1Kh13, 45 and U-7 should be hot-worked at 1100 - 900 °C at strain rates of 1 - 15 sec<sup>-1</sup> to ensure the highest plasticity. There are 2 figures and 7 tables.

Card 5/3

AGEYEV, Nikolay Pavlovich, inzh.; CHERNYAKOVA, I.Z., inzh., red.;  
FREGER, D.P., red. izd-va; BELOGUROVA, I.A., tekhn. red.

[Mechanical properties of steel at high temperatures and  
various rates of deformation] Mekhanicheskie svoistva stali  
pri vysokikh temperaturakh i razlichnykh skorostyakh de-  
formatsii. Leningrad, 1961. 26 p. (Leningradskii dom  
nauchno-tekhnicheskoi propagandy. Seriia: Goriachaia i kholod-  
naia obrabotka metallov davleniem, no.10) (MIRA 15:5)  
(Steel—Testing) (Metals at high temperatures)

188200 1454 1413

27149

S/182/61/000/009/001/005  
D038/D112

AUTHOR: Ageyev, N.P.

TITLE: Effect of an increased temperature and high-speed rate in working by pressure on the resistance to deformation in steels

PERIODICAL: Kuznechno-shtampovochnoye proizvodstvo, <sup>3</sup> no. 9, 1961, 1-4

TEXT: The article describes the results of an investigation on the effect of temperature and speed of deformation on the resistance to deformation in steels in hydraulic and power presses. The test was carried out at the kafedra "Obrabotka metallov davleniyem", Leningradskiy mekhanicheskiy institut (the Department of "Working of Metals by Pressure", Leningrad Mechanical Engineering Institute) on a tensile testing machine developed and designed by the department. Prior to testing, 6 mm diam, 60 mm long specimens were heated to a preset temperature for 20-30 min and then kept for 5-15 min in an electric tubular furnace. The following deformation speeds were used:  $(3-6) \cdot 10^{-3}$ ;  $(5.0-8.0) \cdot 10^{-2}$ ;  $(2.0-4.0) \cdot 10^{-1}$ ;  $1.0-3.0 \text{ sec}^{-1}$  at  $800-1200^{\circ}\text{C}$ , and 3 to 5 specimens were tested at every speed. The

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S/182/61/000/009/001/005  
D038/D112

27149

Effect of an increased temperature...

test results of the 45, Y 7 (U7), and 1X 13 (1Kh13) steels were analyzed. It is stated that F.F. Vitman and N.A. Zlatin (Ref. 4: Vitman, F.F., Zlatin, N.A., Ioffe, B.S., Soprotivleniye deformirovaniyu metallov pri skorostyakh  $10^{-6}$  -  $10^2$  m/sec $^4$  [The resistance to deformation in metals at speeds of  $10^{-6}$  -  $10^2$  m/sec $^4$ ], ZhTF, t. XIX, vyp. 3, 1949) had determined the dependence of hardness on speed deformation in Al, Zn, Pb, and mild steel within a high-temperature range; this was confirmed for a range of non-ferrous metals and steels by L.D. Sokolov (Ref. 3: "Sistematische issledovaniye skorostnoy i temperaturnoy zavisimosti soprotivleniya deformirovaniyu u odnofaznykh metallov" [A systematic investigation into the speed and temperature dependence of resistance to deformation in single-phase metals], Doklady AN SSSR, t. LXX, no. 5, 1950), and for steels by M.A. Zaykov (Ref. 5: Shamets, Ya.V., Zaykov, M.A., Soprotivleniye deformatsii uglero-distykh stalej pri vysokoskorostnoy goryachej prokatke [Resistance to deformation in carbon steels at high-speed rolling], "Izvestiya vysshikh uchebnykh zavedenij chernaya metallurgiya", no. 5, 1959). The correctness of a double logarithmic dependence between the deformation speed and deformation resistance for 08kp (08kp), 40, M 62 (M62), and Y 8A (U8A) carbon steels

Card 2/3

AGEYEV, N.P.; KARATUSHIN, S.I.

Methods for short-time tests of metals of elevated deformation  
rates. Zav. lab. 30 no.5:593-595 '64. (MIRA 17:5)

1. Leningradskiy mekhanicheskiy institut.

ACCESSION NR: AR4036259

S/0137/64/000/003/I036/I036

SOURCE: Referativnyy zhurnal. Metallurgiya, Abs. 3I219

AUTHOR: Ageyev, N. P.

TITLE: Influence of temperature and strain rate on the hardening properties of steels during plastic deformation

CITED SOURCE: Sb. tr. Leningr. mekhan. in-ta, no. 34, 1963, 78-90

TOPIC TAGS: Plastic deformation, strain rate, steel hardening rate, steel deformation resistance

TRANSLATION: The effect of temperature and strain rate (SR) on the hardening rate within the range of the uniform stage of strain was investigated. The hardening rate  $\eta$  was described by the tangent of the slope formed by the positive direction of the tangent to any point of the hardening curve and by the positive direction of the strain axis. The dependence of  $\eta$  on SR may be expressed as  $\eta = k v^{N-M}$ , where  $k = aN/BM$  ( $v$  is the SR,  $N$  and  $M$  are rate exponents which are constant for a given

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ACCESSION NR: ARL036259

temperature and range of rates, and a and B are constants). The temperature dependence of  $\pi$  has the form of an exponential function. In practice, knowing the relationship governing the change of the exponent ( $N-M$ ) with the temperature, one can refine the shape of the hardening curves at any testing temperature by using the dependence of  $\pi$  on the rate and temperature of the strain. Analysis of the dependence of  $\pi$  on SR made it possible to construct diagrams of change of the hardening curves as a function of the testing temperature with the following characteristic regions: I, region of the most pronounced influence of SR on the deformation resistance, plasticity and on the hardening curves as a whole; II, region of less pronounced influence of SR on the deformation resistance and of a slight influence of SR on plasticity; III, region characterized by an insignificant influence of SR on the deformation resistance and by an opposite influence on the plastic properties, owing to an appreciable effect of strain localization; IV, region which covers very high SR and is essentially characterized by the appearance of brittle fracture of the metal when the critical SR is traversed. The proposed dependence of the  $\pi$  criterion on the temperature and SR was experimentally confirmed by several metals (Ni-Si-Mn steel, and the steels 25, U-7, IKhl3, EI6L2). V. Tarant'yev.

DATE ACQ: 17Apr64

SUB CODE: ML

ENCL: 00

Card 2/2

AGEYEV, Nikolay Pavlovich, kand. tekhn.nauk; MEDVEDEV, V.A., red.

[Resistance to deformation of alloyed steels during hot pressure working] Soprotivlenie deformirovaniu legirovannykh stalei pri goriachoi obrabotke davleniem. Lenigrad, 1965. 36 p. (MIRA 18:10)

L 24798-66 EWT(m)/T/EWP(t) IJP(c) JD/JG

ACC NR: AP6011661

SOURCE CODE: UR/0020/66/167/003/0635/0636

AUTHOR: Ageyev, N. V. (Corresponding member); Ignatov, D. V.; Kantor, M. M.

ORG: Institute of Metallurgy im. A. A. Baykov (Institut metallurgii)

TITLE: Electron microscopic and microdiffraction analysis of nonmetallic inclusions  
in molybdenum and its alloys

SOURCE: AN SSSR. Doklady, v. 167, no. 3, 1966, 635-636, and insert facing p. 636

TOPIC TAGS: molybdenum, molybdenum alloy, alloy inclusion, nonmetallic inclusion, electron beam melted alloy

ABSTRACT: The electron microscope is used for studying nonmetallic inclusions in molybdenum and its alloys melted by various methods. The phase composition and distribution of the inclusions were determined in specimens of molybdenum produced by electron-beam melting and in molybdenum alloys containing carbon (0.003-0.021%), titanium (0.02-0.3%) and zirconium (0.01-0.15%), produced by arc melting, and also by fusion melting. The specimens were studied in the cast, deformed and annealed states. The method used for producing the replicas is briefly described. Photomicrographs and diffraction patterns show that the inclusions consist basically

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UDC: 537.533.35:548.4:669.28

L 24798-66

ACC NR: AP6011661

of Mo<sub>2</sub>C molybdenum carbide. This is probably due to the melting conditions and heat treatment of the specimens. The electron-beam melting and annealing were done in a vacuum of  $10^{-4}$ - $10^{-5}$  Hg mm. Oil vapor diffusion pumps were used for producing the vacuum. Apparently the main residual gas consists of the oil vapors which decomposes to form carbon. This carbon diffuses into the metal and forms carbides. The residual gas in this case does not oxidize molybdenum and tungsten as is the case for several other metals (e.g. Al, Ti, Zr, Fe etc.). Molybdenum and tungsten oxides are apparently unstable under these conditions while their carbides are highly stable. Orig. art. has: 3 figures, 1 table. [14]

SUB CODE: 11/ SUBM DATE: 28Aug65/ ORIG REF: 004/ OTH REF: 004/ ATD PRESS:

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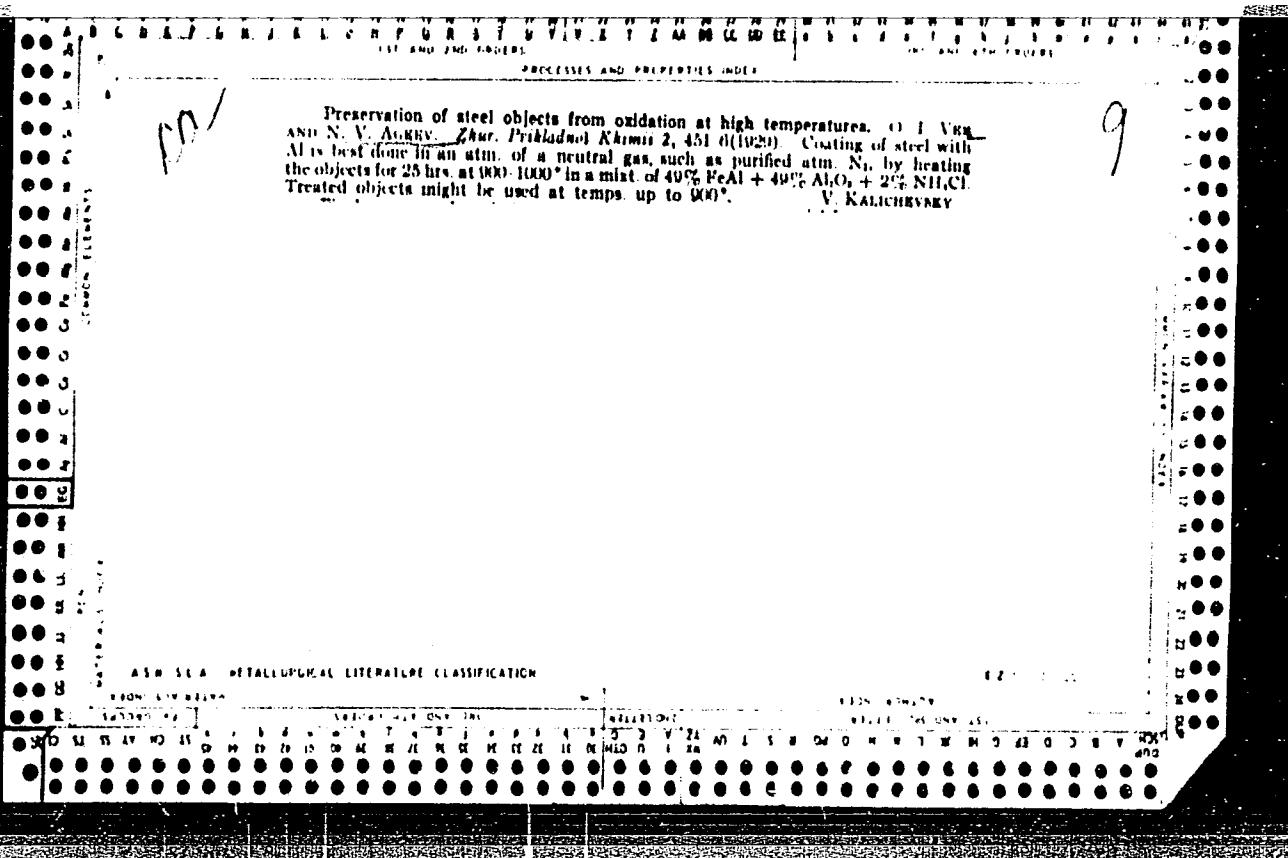
Card 2/2 82

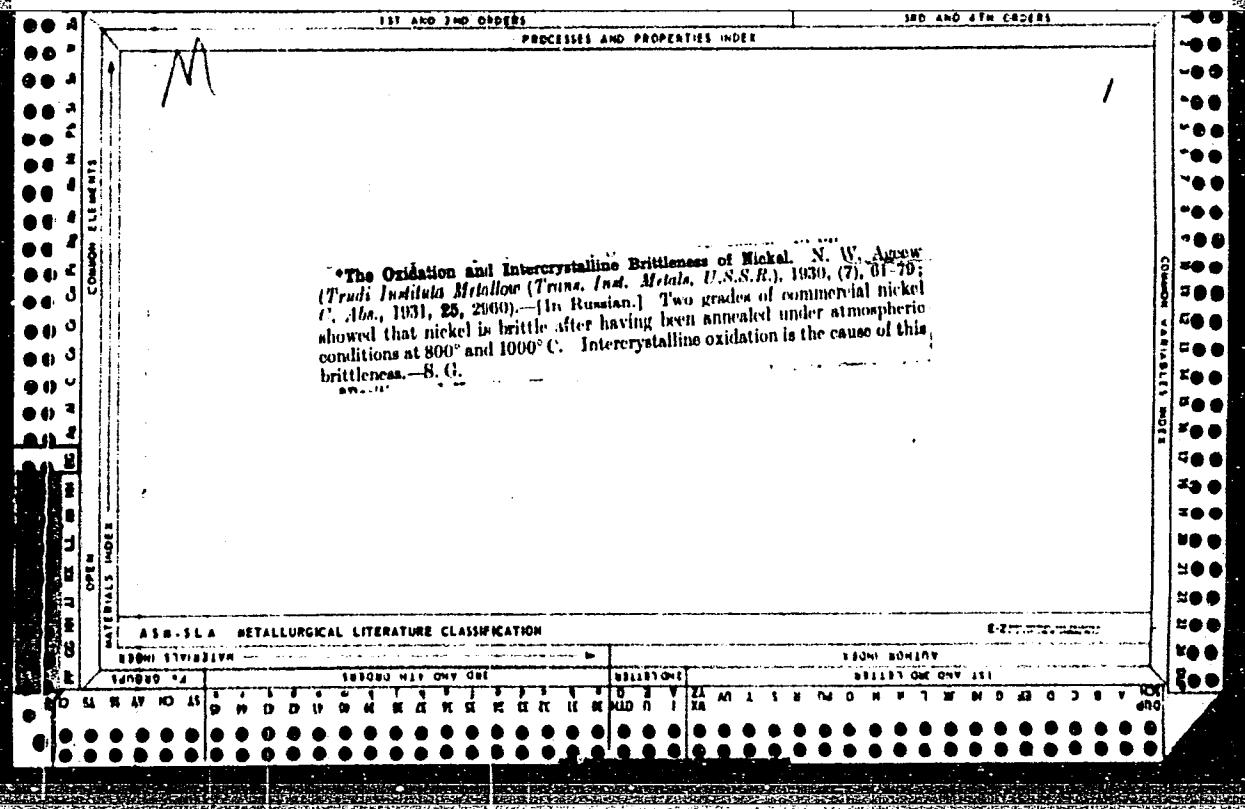
The diffusion of admixtures into steel, and the cellular theory of the structure of metals (according to the work of Professor M. K. Ziegler). N. A. L. V. AND M. ZAMOTIN. *Ann. Inst. Politech. Leningrad* (Sect. Mat. Fiz.) No. 31, 15-25 (1935) (English summary); *J. Inst. Metal.* 64, 558.—A systematic investigation was made of the diffusion of various admixts., both in the solid and liquid states, into mild steel ( $C = 0.08-0.15\%$ ), at temps of 750°, 1000° and 1200°, the duration of each expt. being 3 hrs. In the solid state the degree of penetration of the various admixts. can be arranged on the following decreasing series: at 1000°, C, Pt, ferro-Mo, B, ferro-W, WC, Ni, Au, Mn, ferro-B, Co, ferro-Fe, ferro-chrome, Cr, V, ferro-Si, ferro-Mn, ferro-V, Si, W, Ti. At 1200°, ferro-Si, Mo, Rh, ferro-Mn, Pd, Ru. In the liquid state at 1000°, diffusion was observed with Al, Ce, Cu, no results being obtained with Ag, Bi, Te, Pb, Ca. At 1200° no results were obtained with Ba and Li. At 750° diffusion of Zn could be observed, but not that of Cd. The cellular theory of metal structure developed by the late M. K. Ziegler was examd. in the light of the above results. G. G.

6. 6

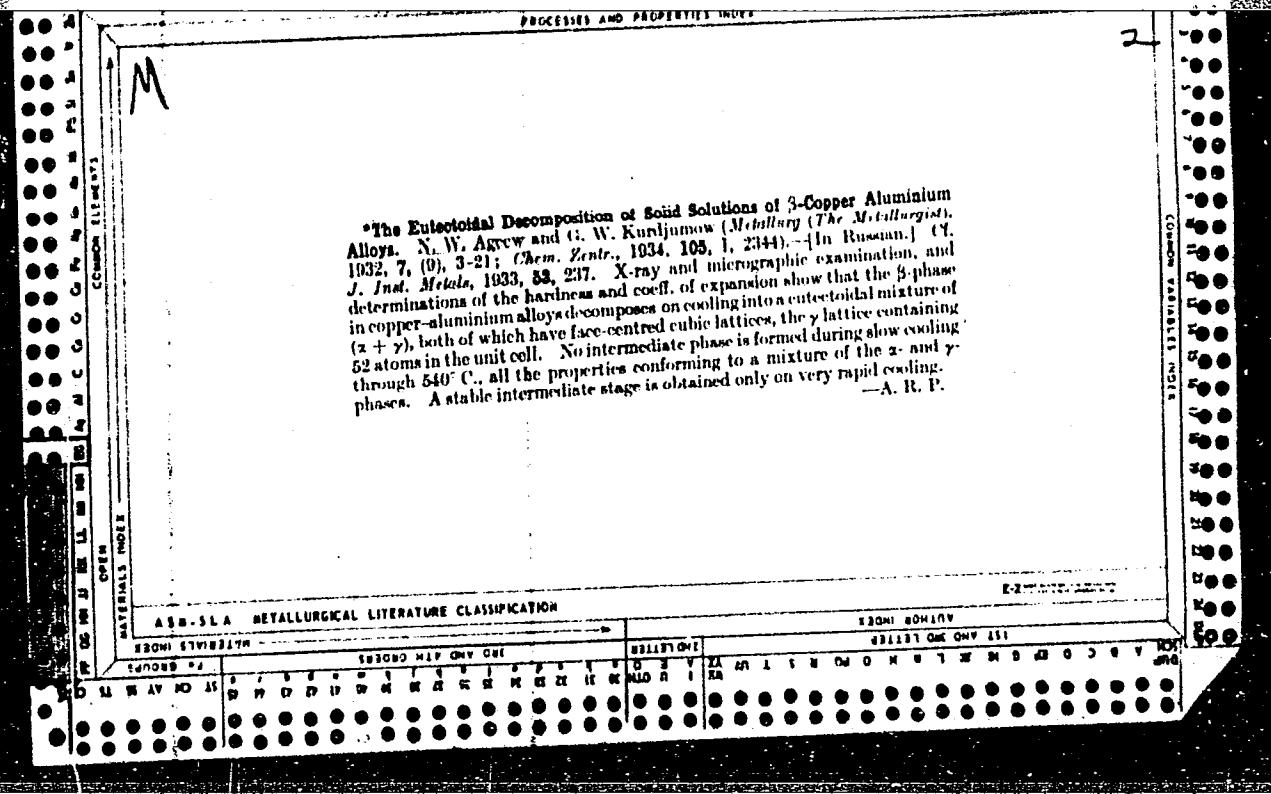
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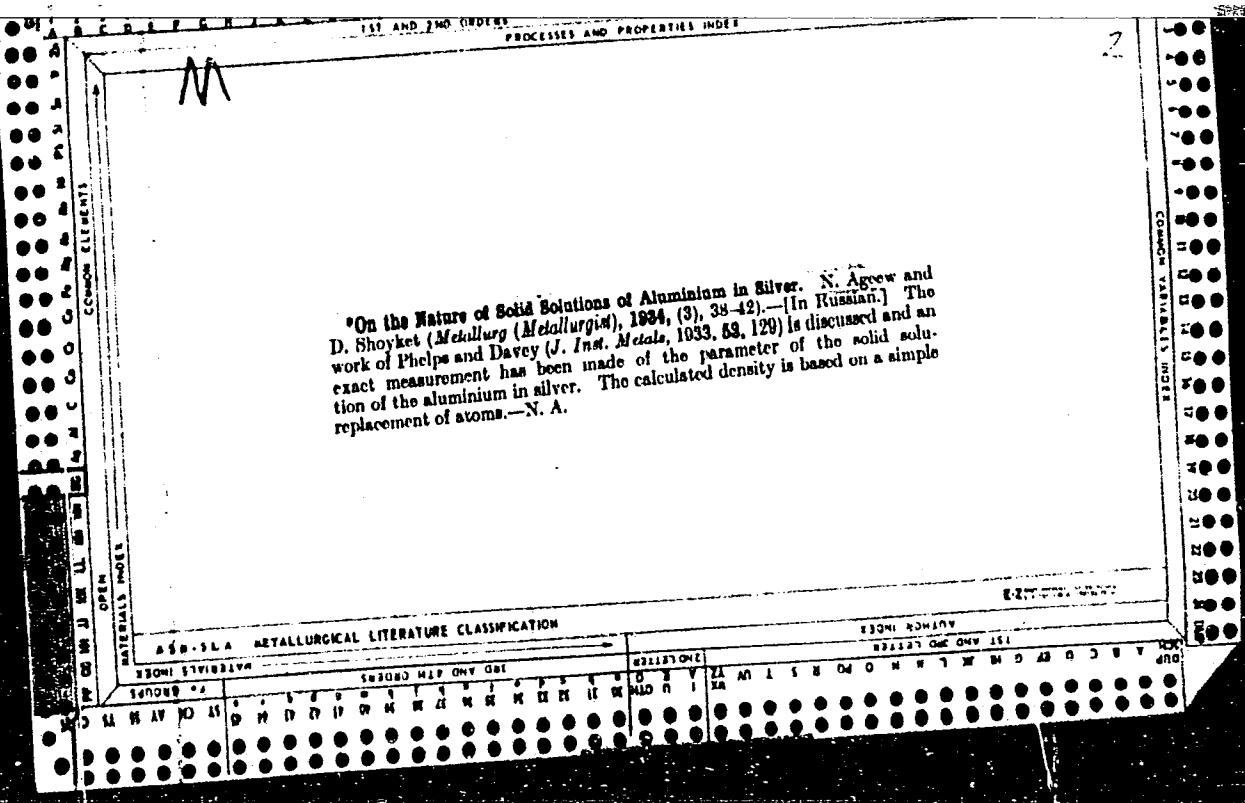


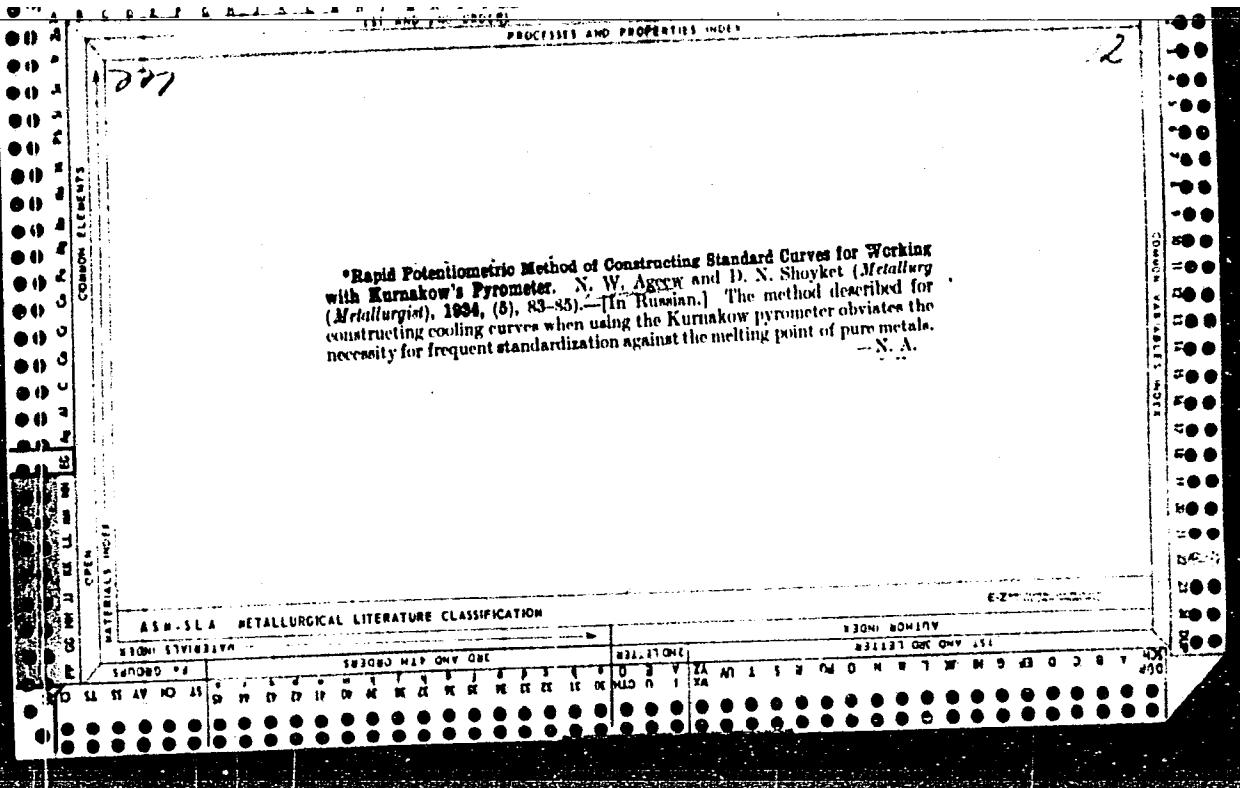


**\*Physicochemical Researches on Solid Solutions of Gold and Copper.** N. S. Kurnakov and N. W. Aggev (*Izvestia Instituta Fiziko-Khimicheskogo Analiza* (Ann. Ind. anal. phys.-fism.), 1933, 6, 25-46; *Chem. Zentral.*, 1934, 108, 11, 1983). [In Russian.] The decomposition of solid solutions of copper and gold into Au<sub>11</sub> and Au<sub>12</sub> below 425°-430° C. has been demonstrated by measurements of the electrical resistance and its thermal coefficient, at temperatures up to 600° C. Dilatometric measurements show that the solid solution range of Au<sub>12</sub> extends from 22 to 40 atomic-% gold and that of Au<sub>11</sub> from 42.2 to 70 atomic-% gold. The formation of the compounds is accompanied by a sharp contraction in volume which does not appear when the alloys are quenched.—A. R. P.

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 1ST AND 2ND COVERS PROCESSING AND PROPERTIES INDEX	3RD AND 4TH COVERS INDEXES 9
<p><b>Diagram of the state of silver alloys with zero to ten per cent aluminum.</b> N. V. Ageev and D. N. Sholikhet. <i>Jour. pol. anal. phys.-chim. (U. S. S. R.)</i> 7, 59-73 (1935); cf. <i>C. A.</i> 28, 6070. Specimens of Ag-Al alloys were held at 650-700° for several days and then either allowed to cool gradually within 15-20 days or water-quenched at definite temps. A diagrammatic analog in the state of the alloys of Cu, Ag and Au with Al was disclosed (cf. Heycock and Neville, <i>C. A.</i> 8, 3849, Stockdale, <i>C. A.</i> 17, 53). The solv. of Al is 0.5% in Cu, 5.4 in Ag and 2.5 in Au. All these systems form <math>\beta</math>-phases stable at high temps. and decompr., on cooling into eutectic mixts. The eutectic mixt. of Cu-Al is stable up to room temp., while that of Ag-Al on cooling forms a new <math>\beta'</math>-phase (<math>Ag_3Al</math>). X-ray study of the <math>\alpha</math>-phase disclosed that the solid soln. is formed by simple substitution of atoms. The <math>\sigma</math>-phase decomposes on heating at 400° into a mixt. of <math>\alpha</math>- and <math>\gamma</math>-phases. A disclosure was made of the existence of a double phase at 400-600° dividing the <math>\beta</math>- and <math>\beta'</math>-phases. The results of the microscopic and x-ray study of the limits of <math>\gamma</math>-phase at various temps. are tabulated.          Chas. Blane       </p>	
<b>ASB-SLA METALLURGICAL LITERATURE CLASSIFICATION</b>	
100001-1198179      1970001-1970002      1A9 ONLY ONE      1000001-1000002      1000003-1000004      1000005-1000006      1000007-1000008      1000009-1000010      1000011-1000012      1000013-1000014      1000015-1000016      1000017-1000018      1000019-1000020      1000021-1000022      1000023-1000024      1000025-1000026      1000027-1000028      1000029-1000030      1000031-1000032      1000033-1000034      1000035-1000036      1000037-1000038      1000039-1000040      1000041-1000042      1000043-1000044      1000045-1000046      1000047-1000048      1000049-1000050      1000051-1000052      1000053-1000054      1000055-1000056      1000057-1000058      1000059-1000060      1000061-1000062      1000063-1000064      1000065-1000066      1000067-1000068      1000069-1000070      1000071-1000072      1000073-1000074      1000075-1000076      1000077-1000078      1000079-1000080      1000081-1000082      1000083-1000084      1000085-1000086      1000087-1000088      1000089-1000090 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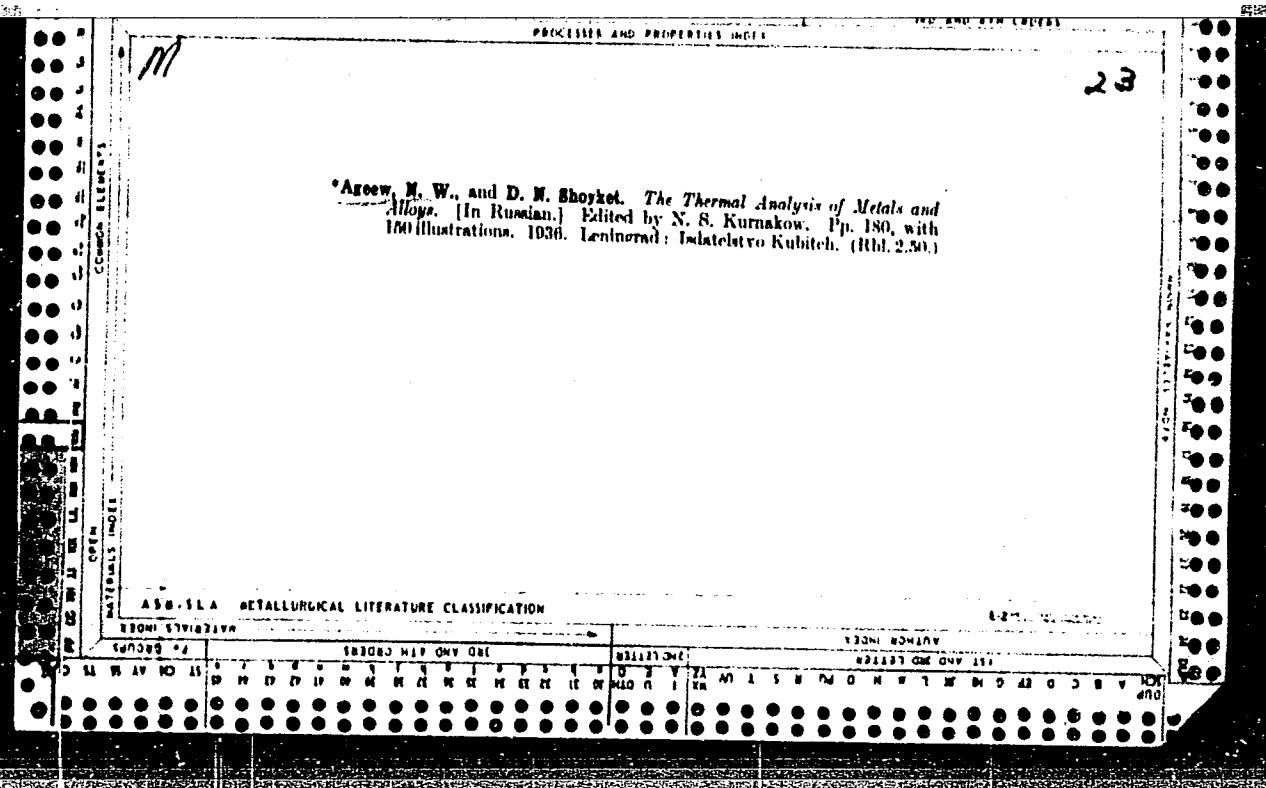
\*The Physico-Chemical Investigation of the Phases of Variable Composition in the Gold-Copper System. N. W. Ageev and D. N. Shoykhet (*Metallurg* (*Metallurgia*), 1933, (7), 86-100).—[In Russian.] The intensity of the reflexes in the Debye röntgenogram, indicates that, in alloys with a nearly stoicheiometric composition, the degree of order is 0.89 for AuCu and 0.92 for AuCu<sub>3</sub>, i.e. about 10% of the atoms are out of place. With the addition of excess of gold or copper to form solid solutions, the degree of order decreases and appears to be smaller than that theoretically possible. The composition-degree of

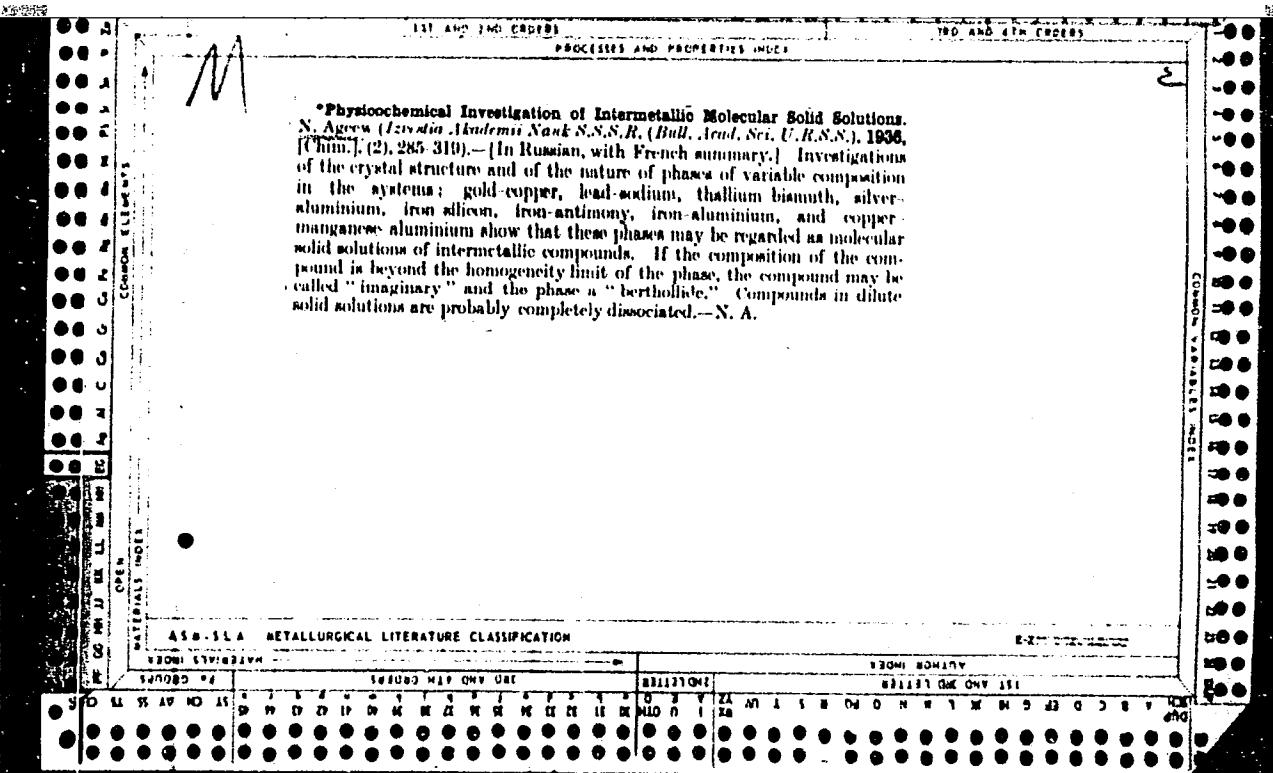
order curves for AuCu and AuCu<sub>3</sub> are similar in character, both being convex towards the copper side. The chief factor which determined the change in properties of solid solutions, is the degree of order in the lattice structure.

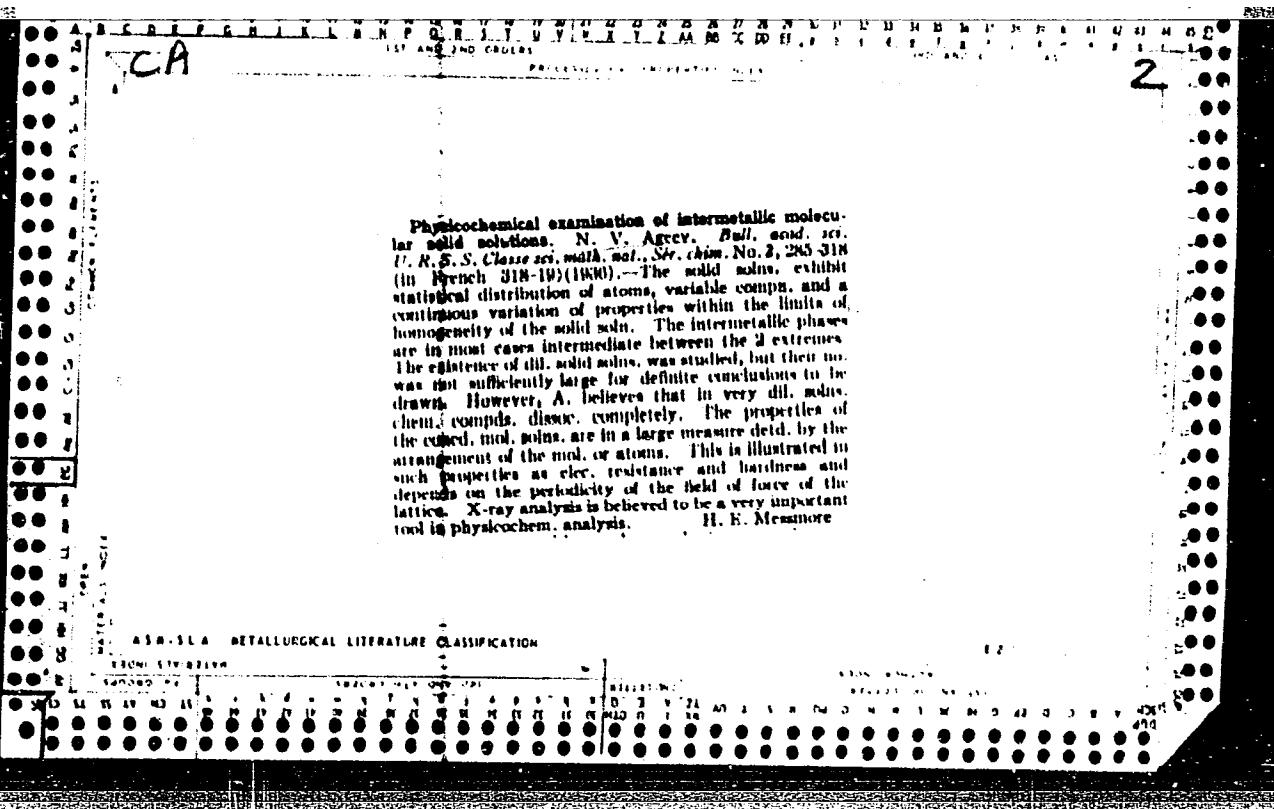
-N. A.

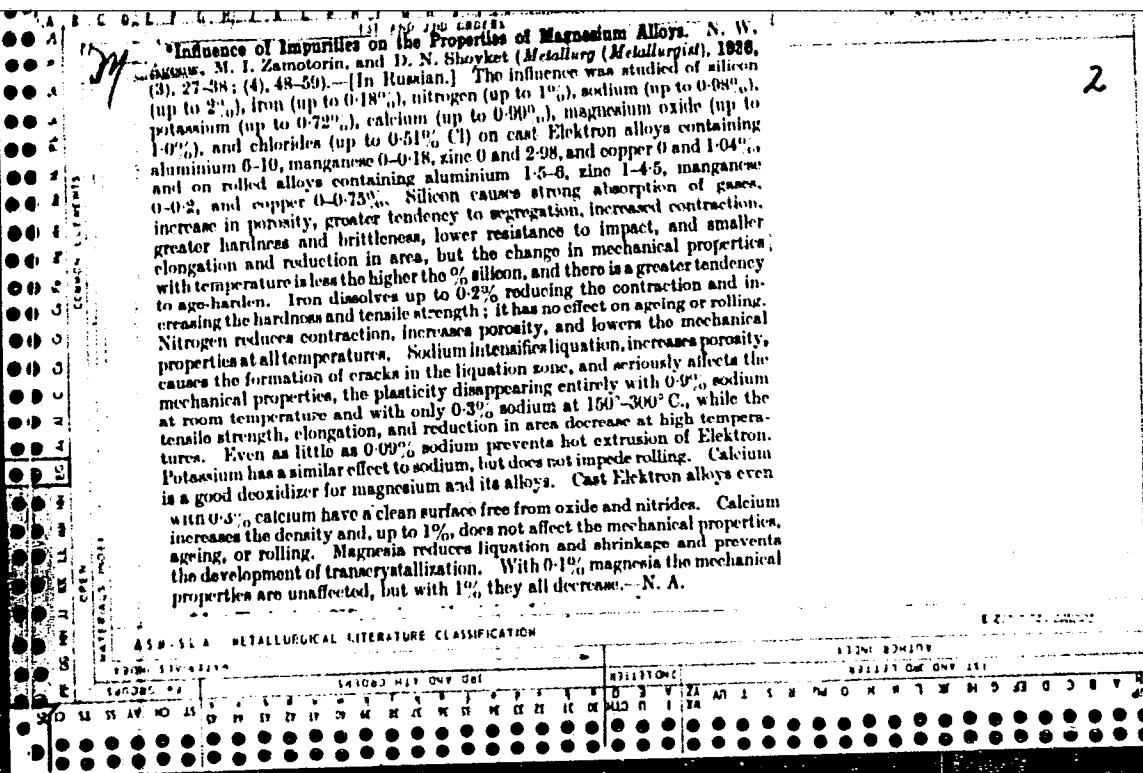
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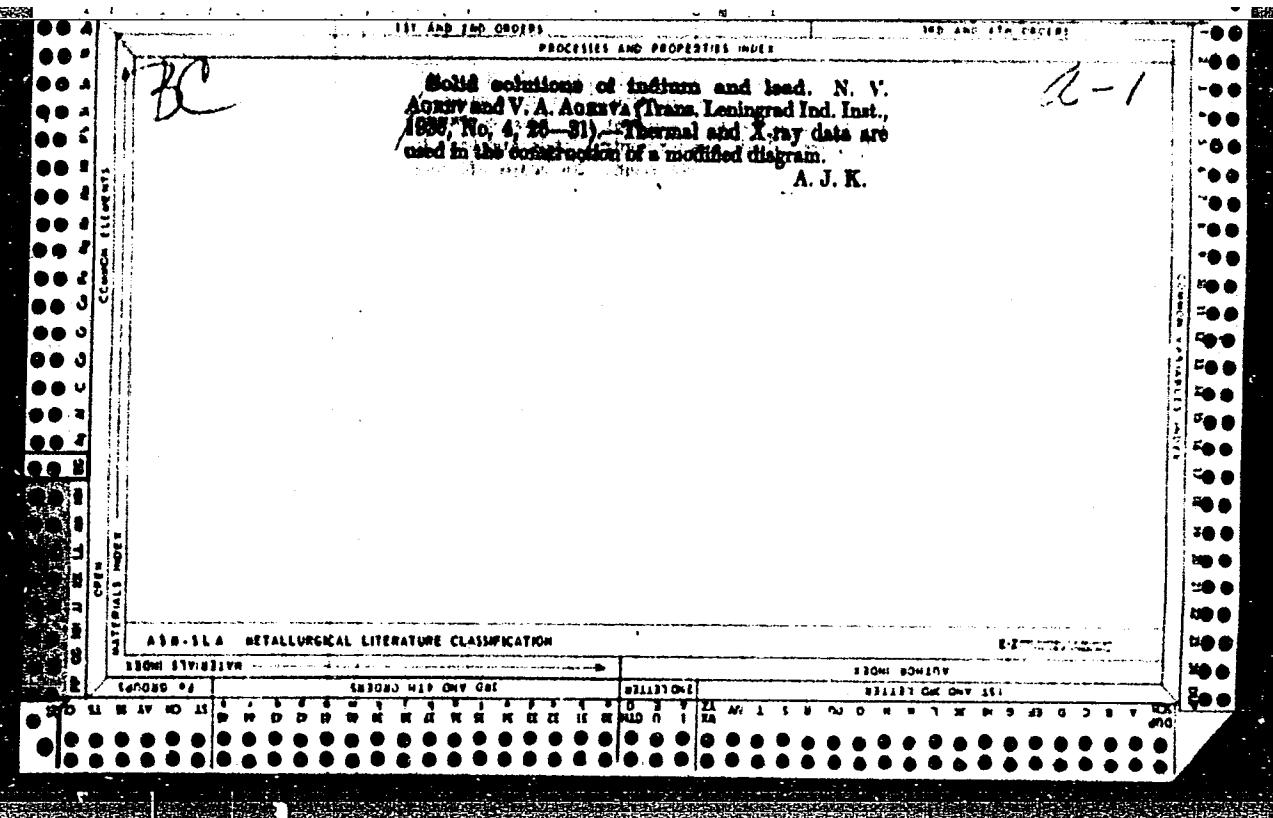
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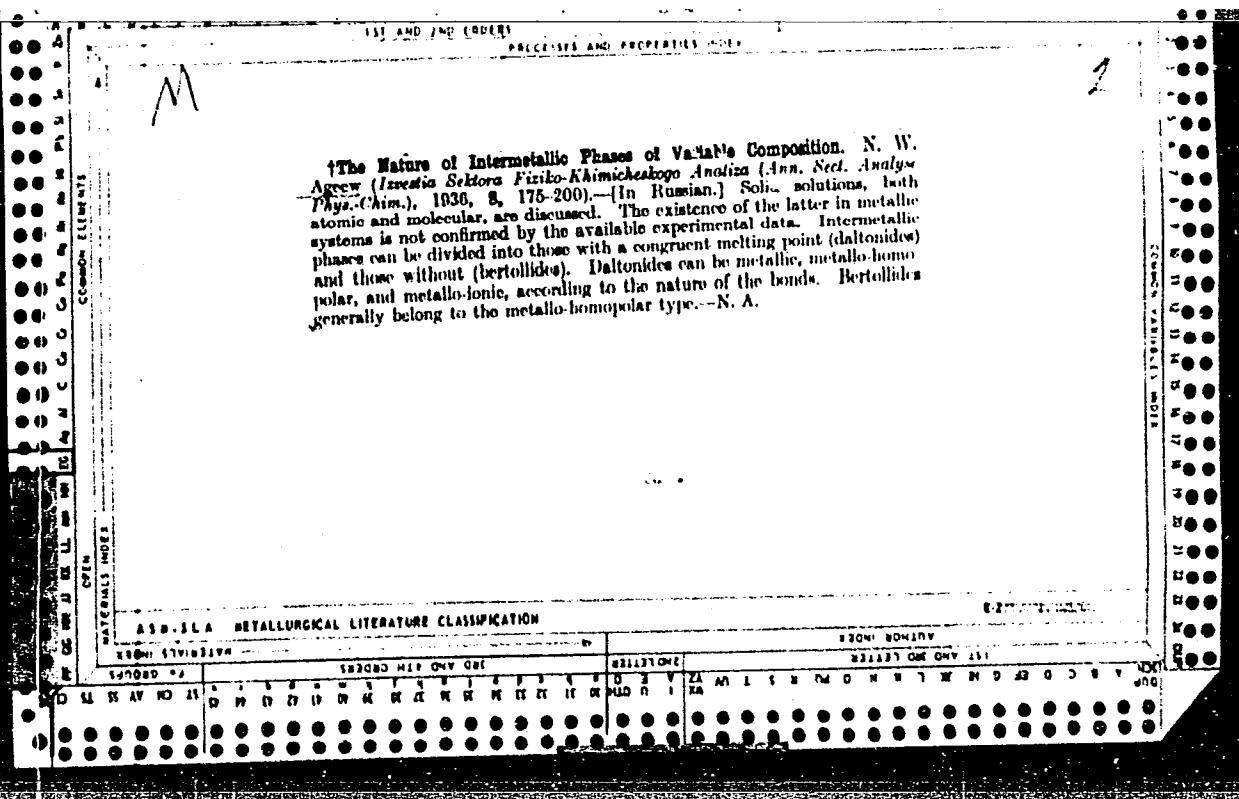








**The Nature of Intermetallic Phases of Variable Composition.** N. W. Agnew (*Izvestia Selskogo Finiko-Khimicheskogo Analiza* (*Ann. Soc. Analys Phys.-Chim.*), 1936, 8, 175-200).—[In Russian.] Solid solutions, both atomic and molecular, are discussed. The existence of the latter in metallic systems is not confirmed by the available experimental data. Intermetallic phases can be divided into those with a congruent melting point (daltonides) and those without (bertollides). Daltonides can be metallic, metallo-homo-polar, and metallo-ionic, according to the nature of the bonds. Bertollides generally belong to the metallo-homopolar type.—N. A.



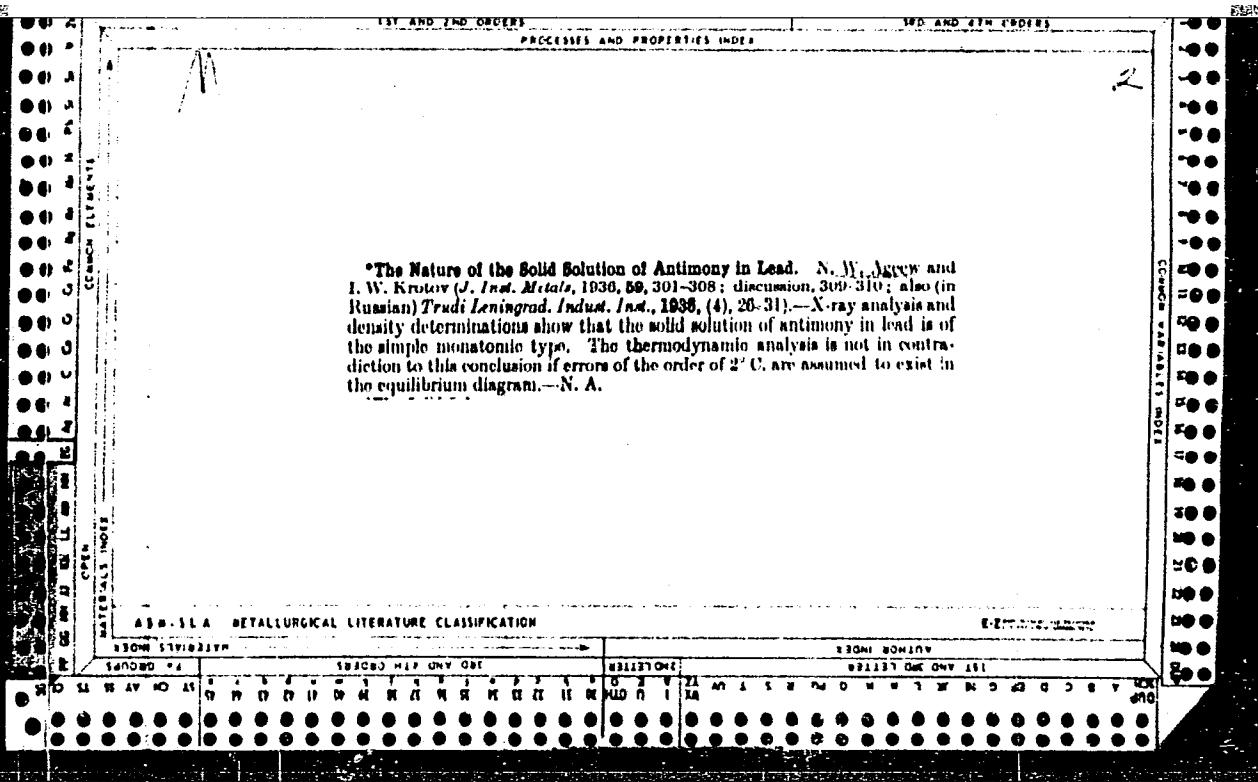
**PROCESSED AND PROPRIETARY INDEX**

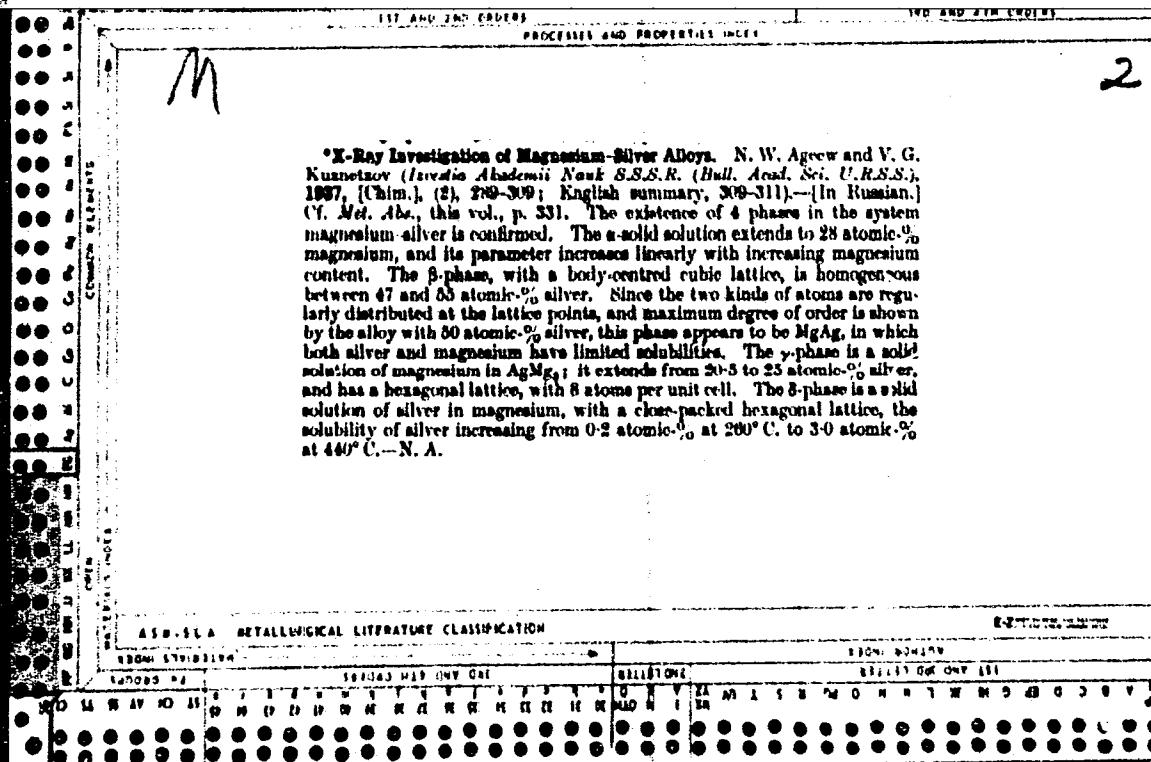
The nature of molecular phases of variable composition in the system: gold-copper. N. V. Agreva and D. N. Shokhlet. *Ann. sovetsk. soosl. phys.-chim., Inst. chim. pris.* (U. S. S. R.) 9, 129-46 (1936); cf. *C. A.* 29, 4049; Kurnakov and Agreva, *Ibid.* 6, 23 (1933).—X-ray examined by the wire and powder method of annealed AuCu and AuCu<sub>3</sub> in the Au-Cu system showed a cryst. lattice with a random distribution of the Au and Cu atoms. Similar results were obtained for Al-Fe alloys by Bradley and Jay (*C. A.* 22, 5532) and for Al-Mn alloys by Heusler (*C. A.* 22, 3307). AuCu and AuCu<sub>3</sub> do not form a continuous series of solid solns. The character of the property changes in the formation of solid solns. indicates a complete analogy with the change of the degree of regularity. It proves that the chief factor governing the change of properties of a solid soln. with the change of concn. is the disturbance of the orderly distribution of atoms in it.

Chas. Blanc

**480.16A METALLURGICAL LITERATURE CLASSIFICATION**

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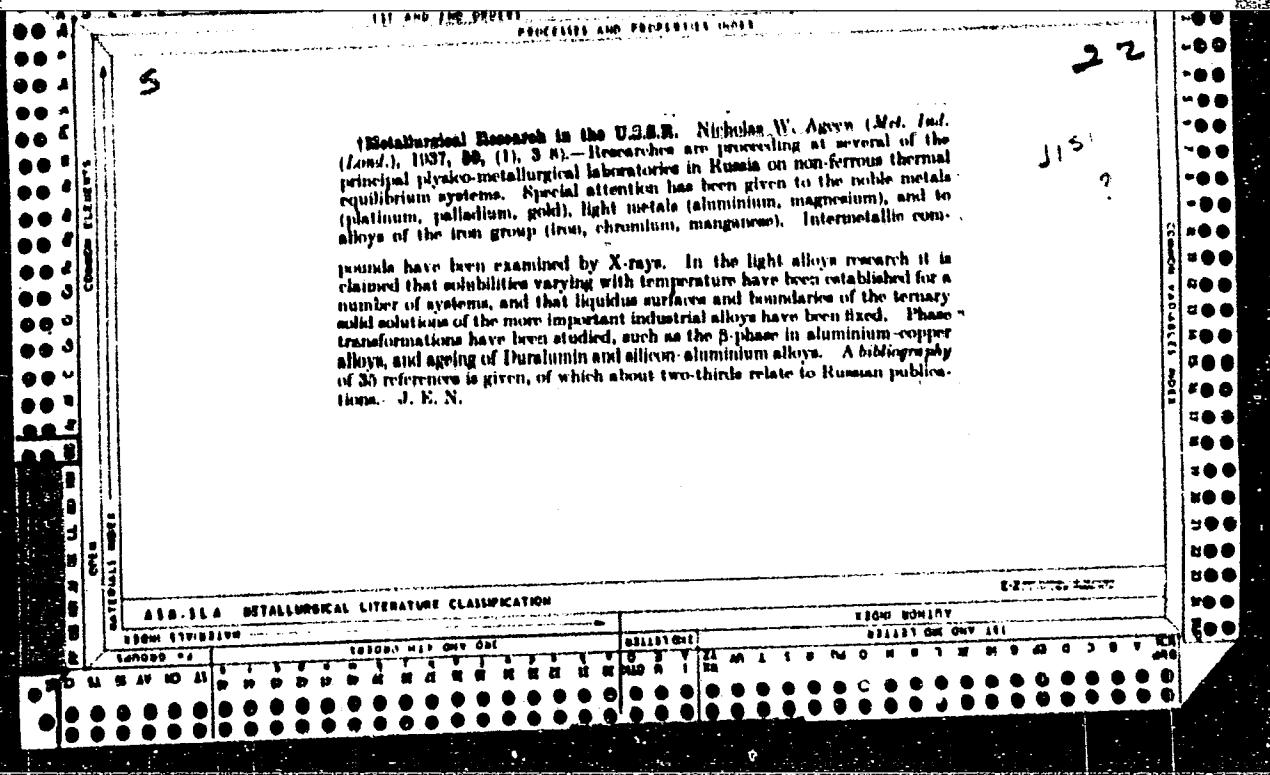


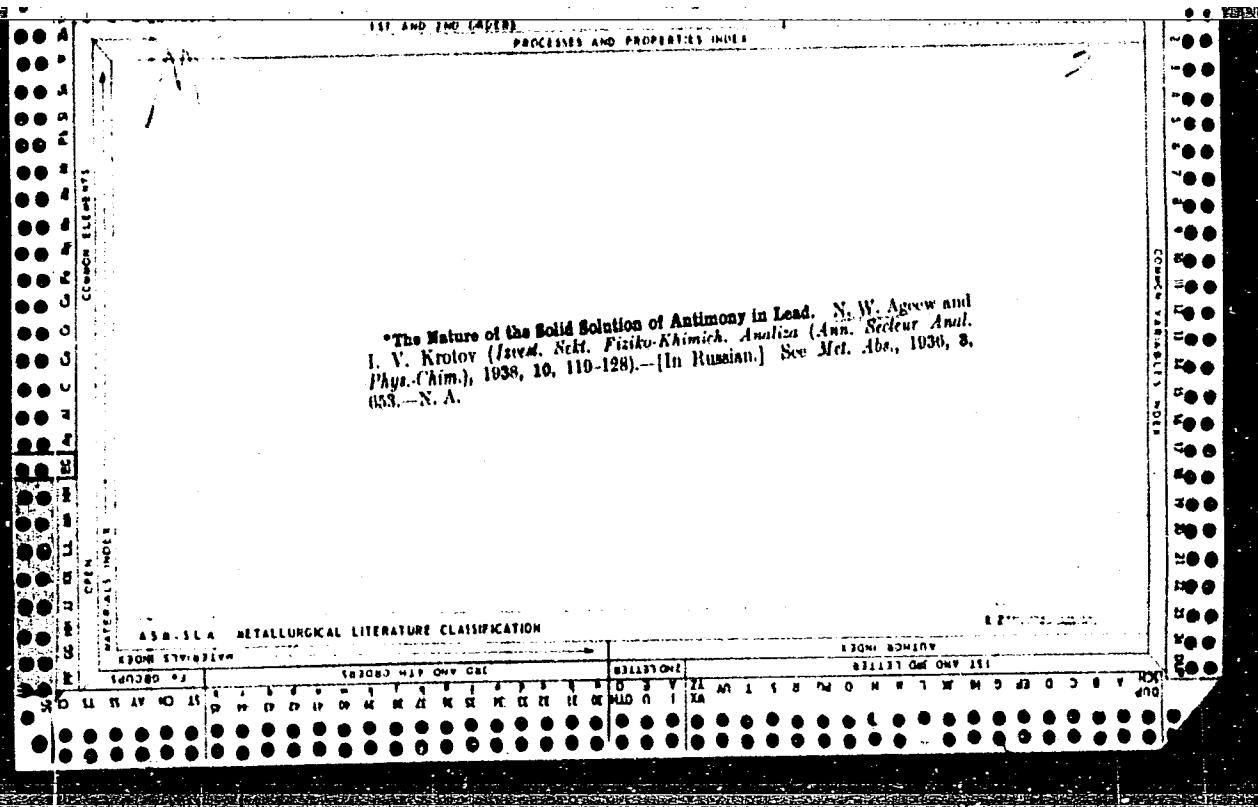


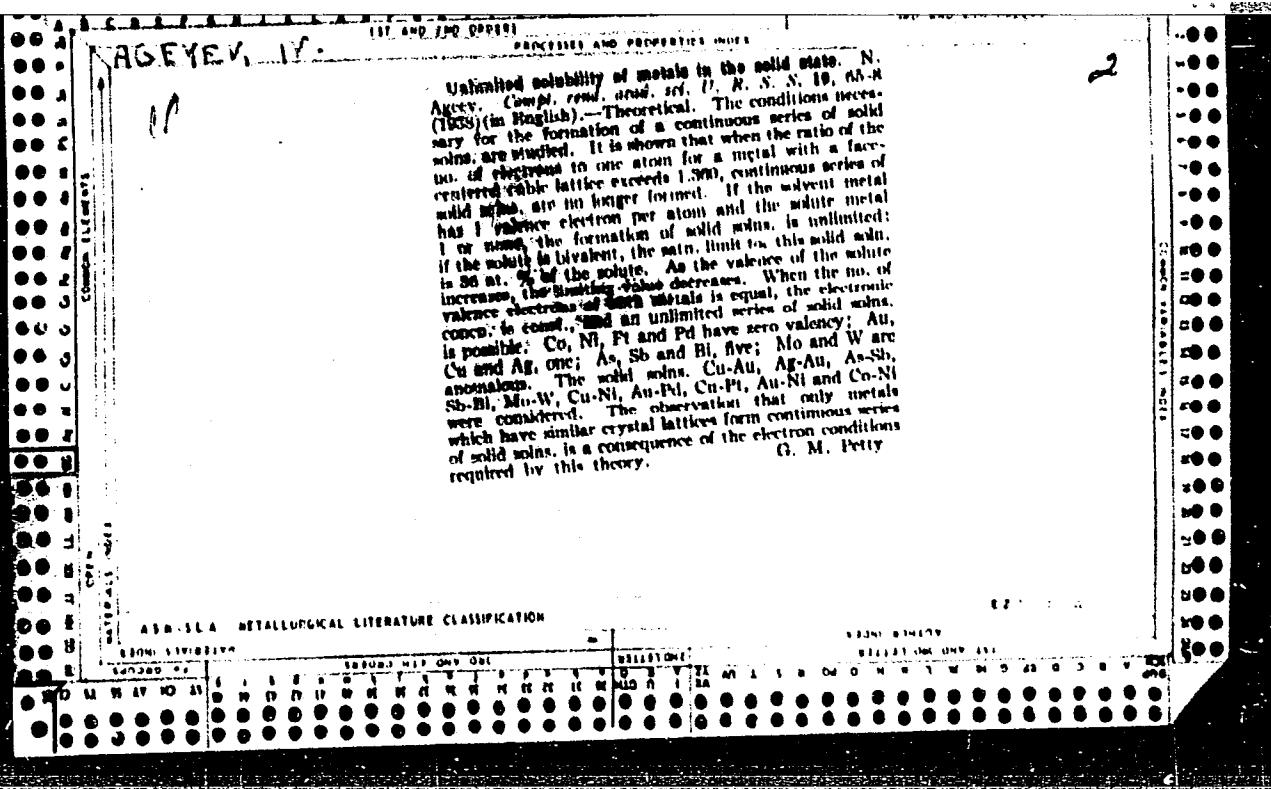
**X-Ray Study of Platinum-Ruthenium Alloys.** N. W. Agnew and V. G. Kusnezov (*Izv. Akad. Nauk S.S.R. (Bull. Acad. Sci. U.R.S.S.)*, 1937, [Chem.], (4), 783-786).—[In Russian, with English summary.] Cf. *Met.*, 1937, 4, 116. An x-ray study of platinum-ruthenium alloys by the Debye method showed the formation of solid solutions up to 70 atomic-% ruthenium. The lattice constant decreased from 3.915, Å. (pure platinum) to 3.82, Å.—N. A.

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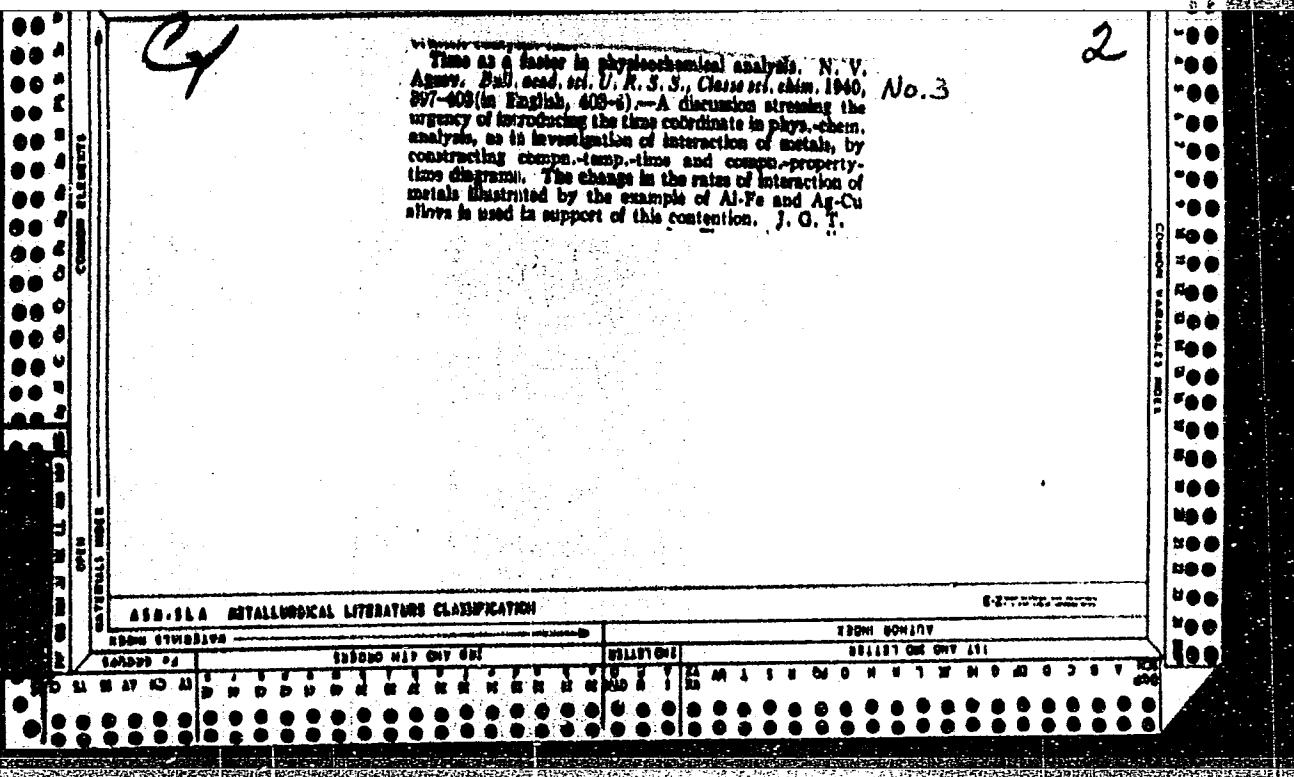
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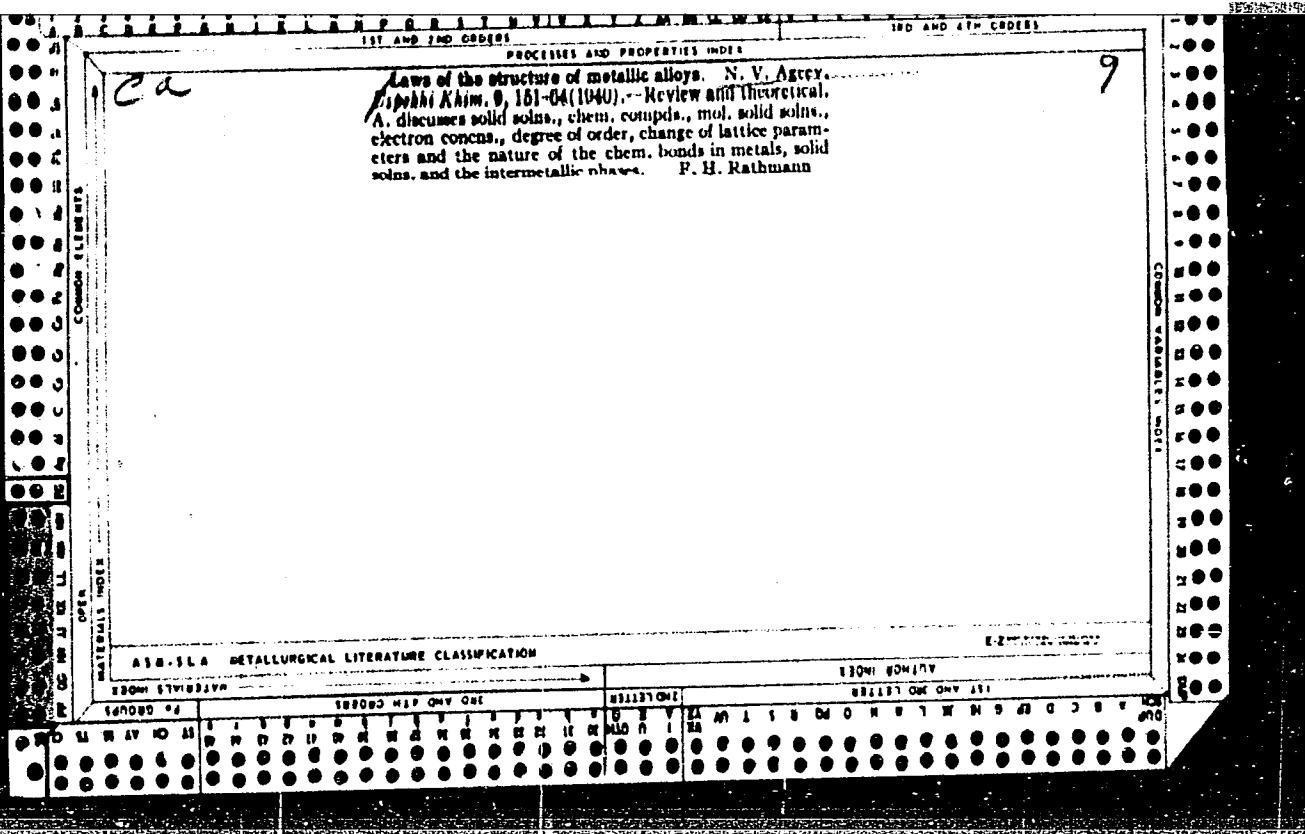
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No. 3

Time as a factor in physicochemical analysis. N. V. Agarwala, *Bull. Acad. sci. U. R. S. S., Classe sci. chim.*, 1940, 397-403 (in English, 403-6).—A discussion stressing the urgency of introducing the time coordinate in phys.-chem. analysis, as to investigation of interaction of metals, by constructing compo.-temp.-time and compo.-property-time diagrams. The change in the rates of interaction of metals illustrated by the example of Al-Fe and Ag-Cu alloys is used in support of this contention. J. G. T.

2





**The Structure of the  $\beta$  Phase in Gold-Zinc Alloys.** N. W. Agew and D. N. Shuykhet (*Zvez. Sekt. Fiziko-Khimich. Analiza (Ann. Sector Anal. Phys.-Chim.)*, 1940, 18, 165-170). [In Russian.] The limits of homogeneity of the  $\beta$  phase were found by microscopic examination to be 47.5 and 52.0 atomic-% gold. Debye X-ray examination of the alloy with 50.49 atomic-% gold confirmed that the  $\beta$  phase has a caesium chloride type of structure with 2 atoms per unit cell. The calculated density checks closely with the measured value. The position of the atoms in the  $\beta$  phase was calculated. The maximum degree of order occurs at the stoichiometric proportion of Au : Zn = 1 : 1. The order  $\rightarrow$  disorder transformation sets in on heating above 500° C., but does not proceed to completion up to the melting point of 725° C. A. B.

**ASH-SLA METALLURGICAL LITERATURE CLASSIFICATION**

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<i>M</i>						<i>Z</i>																									
<p><b>*The Structure of the <math>\beta</math> and <math>\epsilon</math> Phases in the Copper Antimony System.</b>      N. W. Agreew and E. S. Makarov (<i>Izv. Akad. Nauk SSSR, Fiziko-Khimich. Analiza</i>, <i>Ann. Selsk. Akad. Phys.-Chim.</i>, 1940, <b>18</b>, 171-176).—[In Russian.] Alloys with 60-70 wt.% copper, investigated by microscopic examination and the Debye X-ray method, confirmed in general the equilibrium diagram of Murakami and Shibata (<i>Met. Abs.</i>, 1937, <b>4</b>, 36). The <math>\epsilon</math> phase is homogeneous between 67.89 and 68.08% copper, which is more on the antimony side than is given by M. and S. The eutectoid point is situated at about 62.0% copper. Alloys with 60.00 to 64.04% copper consisted of the homogeneous <math>\beta</math> phase, the limit on the copper side being at 65% copper. The <math>\epsilon</math> phase, in agreement with Morris-Jones and Evans (<i>Met. Abs. (J. Inst. Metals)</i>, 1928, <b>39</b>, 538), was found to have a hexagonal close-packed lattice with <math>a = 2.723</math> 2.745, <math>c = 4.322</math>-4.340 Å. The structure of quenched specimens of the <math>\beta</math> phase was found to be cubic with 16 atoms per unit cell and a parameter of 5.914 Å. The <math>\beta</math> phase has an orderly arrangement of atoms resembling the <math>FeAl_3</math> structure, and corresponds to the formula <math>Cu_{17}Sb_4</math> (<math>Cu_3Sb</math>). A. B.</p>																															
<p style="text-align: center;">ASA-SLA METALLURGICAL LITERATURE CLASSIFICATION</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 15%;">SEARCHED</td> <td style="width: 15%;">INDEXED</td> <td style="width: 15%;">SERIALIZED</td> <td style="width: 15%;">FILED</td> <td style="width: 15%;">SEARCHED</td> <td style="width: 15%;">INDEXED</td> <td style="width: 15%;">SERIALIZED</td> <td style="width: 15%;">FILED</td> </tr> <tr> <td colspan="4" style="text-align: center;">1930-33 MFP ONLY ONE</td> <td colspan="4" style="text-align: center;">1931-33 MFP ONLY ONE</td> </tr> <tr> <td colspan="8" style="text-align: center;">MAY 1965</td> </tr> </table>								SEARCHED	INDEXED	SERIALIZED	FILED	SEARCHED	INDEXED	SERIALIZED	FILED	1930-33 MFP ONLY ONE				1931-33 MFP ONLY ONE				MAY 1965							
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11

M  
THE SOLID SOLUTION OF SODIUM IN LEAD. N. W. AGEEV AND . YA. TALYZIN  
(IZVEST. FIZ. FIZ. IZMICH. ANALIZA. (ANAL. SECTEUR MATER. PHYS. CHIM.) 1940  
13, 251-255) (In Russian) The solid solubility of sodium in lead was  
investigated by X-rays (Preston-type camera with copper radiation), sp. gr.  
measurements, and Brinell hardness tests. In spite of the fact that the atomic  
radius of sodium is larger than that of lead, the lattice parameter of lead  
decreases as the sodium goes into solution. The limiting solubility of sodium  
in lead at 290°C was found to be 1.37 wt. %. The solid solution is of the sim-  
ilar substitution type. Density measurements gave results agreeing with the X-ray  
determination, while the hardness test gave a somewhat lower value for the sol-  
ubility. The complete solubility curve was constructed. It shows that the  
solid solubility of sodium in lead falls to 0.45 wt. --% at room temperature.

#### 1.1.1.4 METALLURGICAL LITERATURE CLASSIFICATION

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*Khimija Metallicheskikh Splavov. (The Chemistry of Metallic Alloys.)* By N. A. Agren. 15 x 22 cm. Pp. 120, with 82 illustrations. 1941. Moscow and Leningrad: Izdatel'stvo Akademii Nauk S.S.R. (6 R., 35 k.)

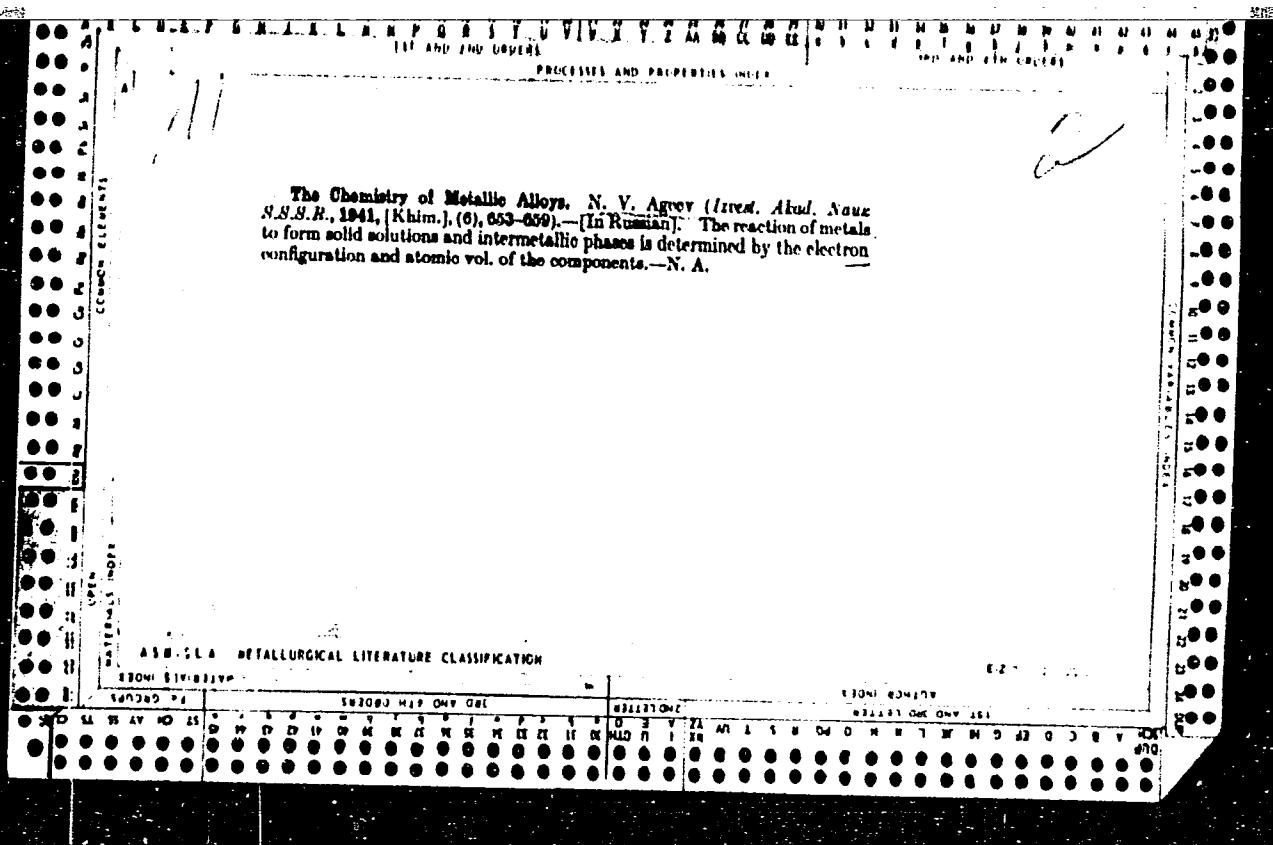
One's first impression on glancing through Professor Agree's monograph is that the simplest way of describing it will be as the Russian equivalent of Dr. Hume-Rothery's "Structure of Metals and Alloys." Both have the same format and the same number of pages and both cover very much the same ground. There is a difference of emphasis, however, for whereas Dr. Hume-Rothery deals at length with primary solid solutions, Professor Agree devotes a large part of his space to a discussion of intermediate phases. But it is not wise to press the comparison of the two books too far, since Professor Agree's monograph is intended primarily as a connected account of the work on alloys on which he has himself been engaged during the last 15 years.

Professor Agre was a pupil of the famous Russian chemist N. S. Kurukov, and since 1925 has carried on many studies of metallic systems by X-rays and by the methods of physico-chemical analysis associated with the use of X-rays. Particularly has he been preoccupied with the subject of "daltoides," which he has defined as follows: "Daltoides is the name given to a phase based on an intermetallic compound which contains compositions with the general formula  $M_2M'$ , however, the composition of the phase may vary, depending on the limits of the phase behavior of the system." In his article on the properties of the copper-aluminum system, the author gives a detailed description of the daltoides in the silver-zinc system, and his account of intermetallics has been described in the monograph "Intermetallics, from Aluminides to Carbides," which he has investigated himself. His recent work on the ternary iron-nickel-bertholdite system has shown that a daltoides (nickel-antimony) with a bertholdite structure occurs in the intermediate regions of solid solutions, and he concludes the thesis that there is no true binary daltoides in either of the two types of phase. It is proposed that continuous solid solutions between daltoides and bertholdites should be called Kurukov phases.

## ASH-SEA METALLURGICAL LITERATURE CLASSIFICATION

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C.A. : Vol. 38, 20 MAR 44		PROCESSES AND PROPERTIES INDEX																			
Ca		9																			
<p>The pyrophoric properties of alloys of the system Mn-Sb. N. V. Ageev and B. S. Makarov. <i>Bull. acad. sov. R. S. S.</i>, classe sci. chim., 1943, 74-A.—The most pyrophoric alloy is one contg. 41.8 wt. % Sb, corresponding to Mn<sub>3</sub>Sb. The constituents are fused under molten KCl-NaCl, cast at 0.01°, and allowed to cool without further treatment. Addn. of 1% Mg almost completely suppresses the pyrophoric properties; 1% Na slightly increases them, and Li, K, Be, Ca and Zn are without effect. The alloy cannot be used in an ordinary lighter, since it must be struck a blow on the edge to produce a spark.</p> <p>H. M. Lester</p>																					
<p>ASTM-SEA METALLURGICAL LITERATURE CLASSIFICATION</p>																					
ECONOMICS		GENERAL		STRUCTURE		TESTS		PROCESSES		PROPERTIES		COMBINATION									
1943-1944		1943-1944		1943-1944		1943-1944		1943-1944		1943-1944		1943-1944									
W	M	A	V	H	D	S	T	C	R	P	N	O	I	W	M	D	O	S	V	A	9

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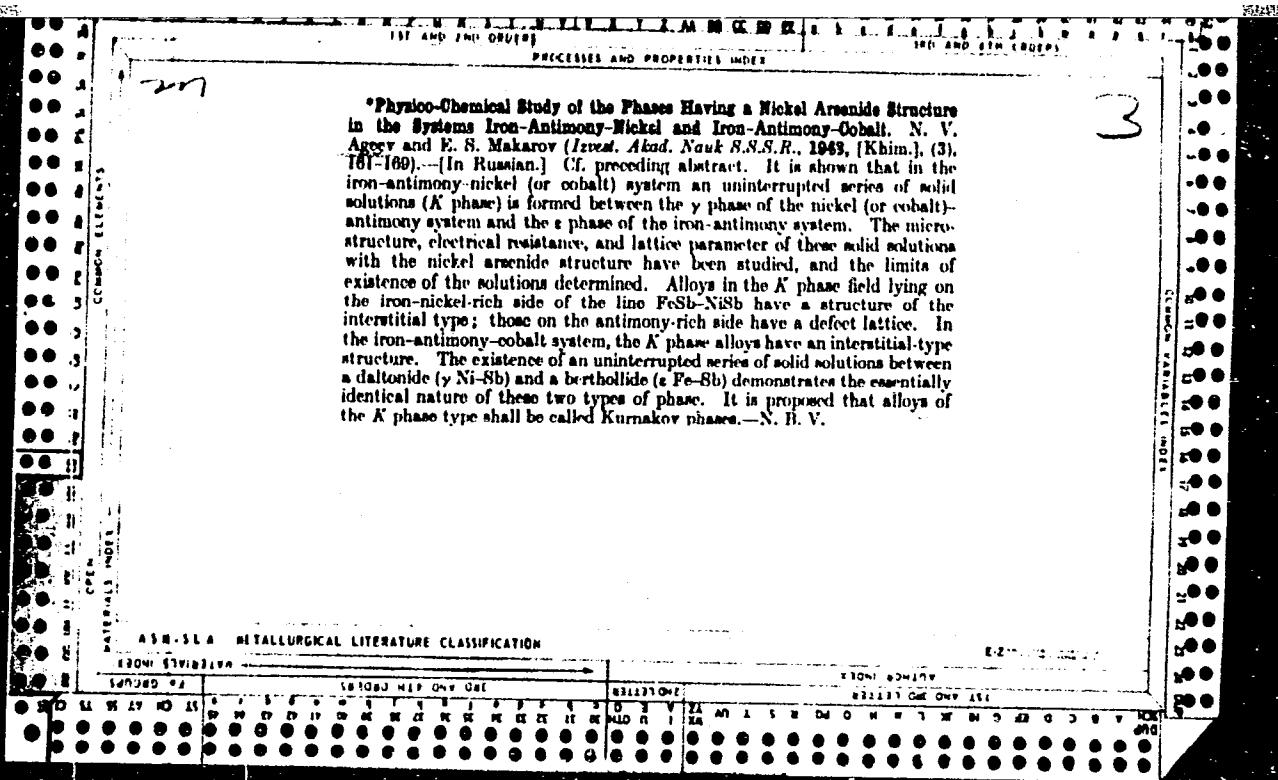
**\*Physico-Chemical Study of the Phases Having a Nickel Arsenide Structure in the Systems Iron-Antimony, Cobalt-Antimony, and Nickel-Antimony.** N. V. Agreyev and E. S. Makaryan [Inzvest. Akad. Nauk S.S.R., 1943, (Khim.), (2), 87-97].—[In Russian.] (Y. Compt. rend. [Doklady] Acad. Sci. U.R.S.S., 1943, 23, 20; Met. Abs., this vol., p. 110. The phases having a nickel arsenide structure in the nickel-antimony, cobalt-antimony, and iron-antimony systems have been studied by means of X-ray and microstructural examination and by determinations of electrical resistance and density. (1) The  $\gamma$  phase of the nickel-antimony system is found to exist over the range 46.4-54.4 at.-% antimony; it includes the compound Ni<sub>3</sub>Sb and the phase is therefore a daitonite. Comparison of the density of the alloys as measured directly and as derived from lattice spacings shows that  $\gamma$  phase

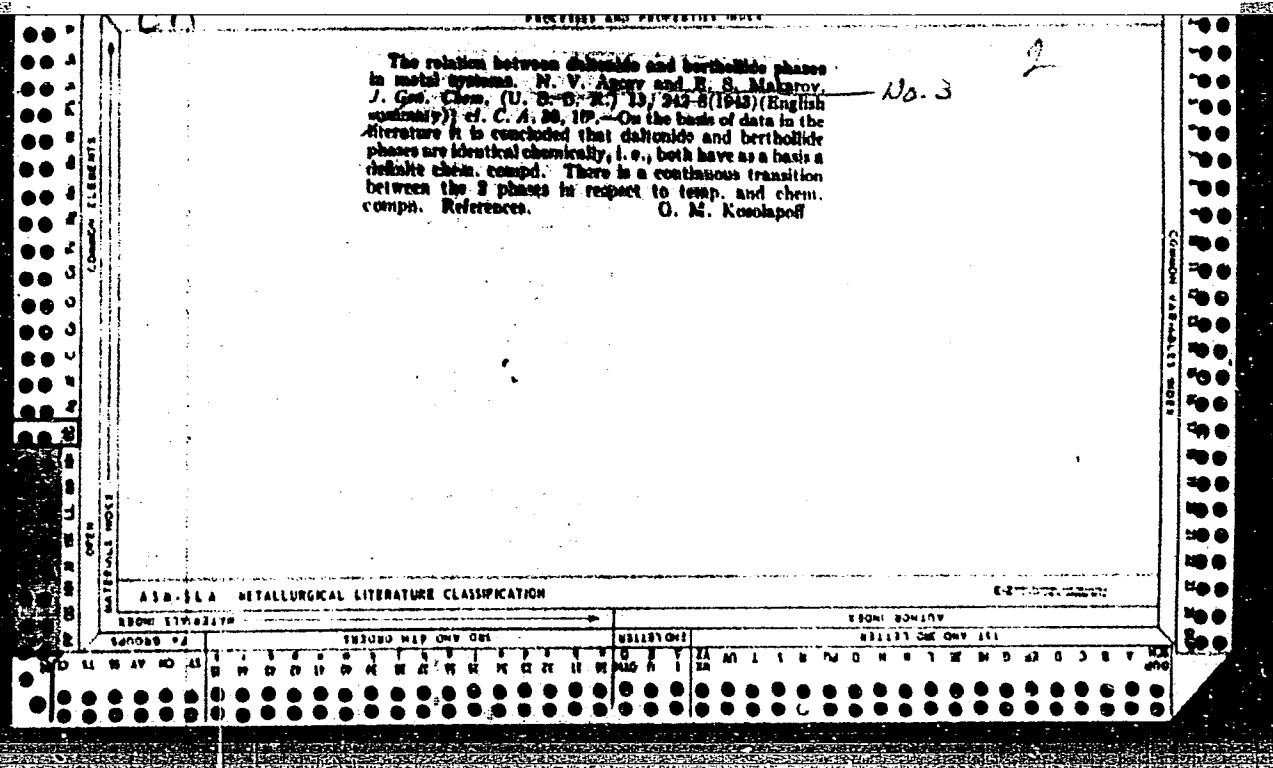
alloys on the nickel-rich side of NiSb have structures of the interstitial type, while those on the antimony-rich side have structures of the defect type. (2) The  $\gamma$  phase of the cobalt-antimony system lies in the range 43.4-49.2 at.-% antimony; this range does not embrace the compound CoSb and the phase is therefore a berthollide. It has a structure of the interstitial type. (3) The  $\epsilon$  phase of the iron-antimony system exists over the range 42-48 at.-% antimony and is likewise a berthollide, being formed by the intrusion of iron atoms interstitially into the lattice of the hypothetical compound FeSb. The hardness, heat of formation, melting point, and interatomic distances of the three phases are compared, and the view is advanced that the strength of chemical linkage decreases in the order: NiSb > CoSb > FeSb.—N. B. V.

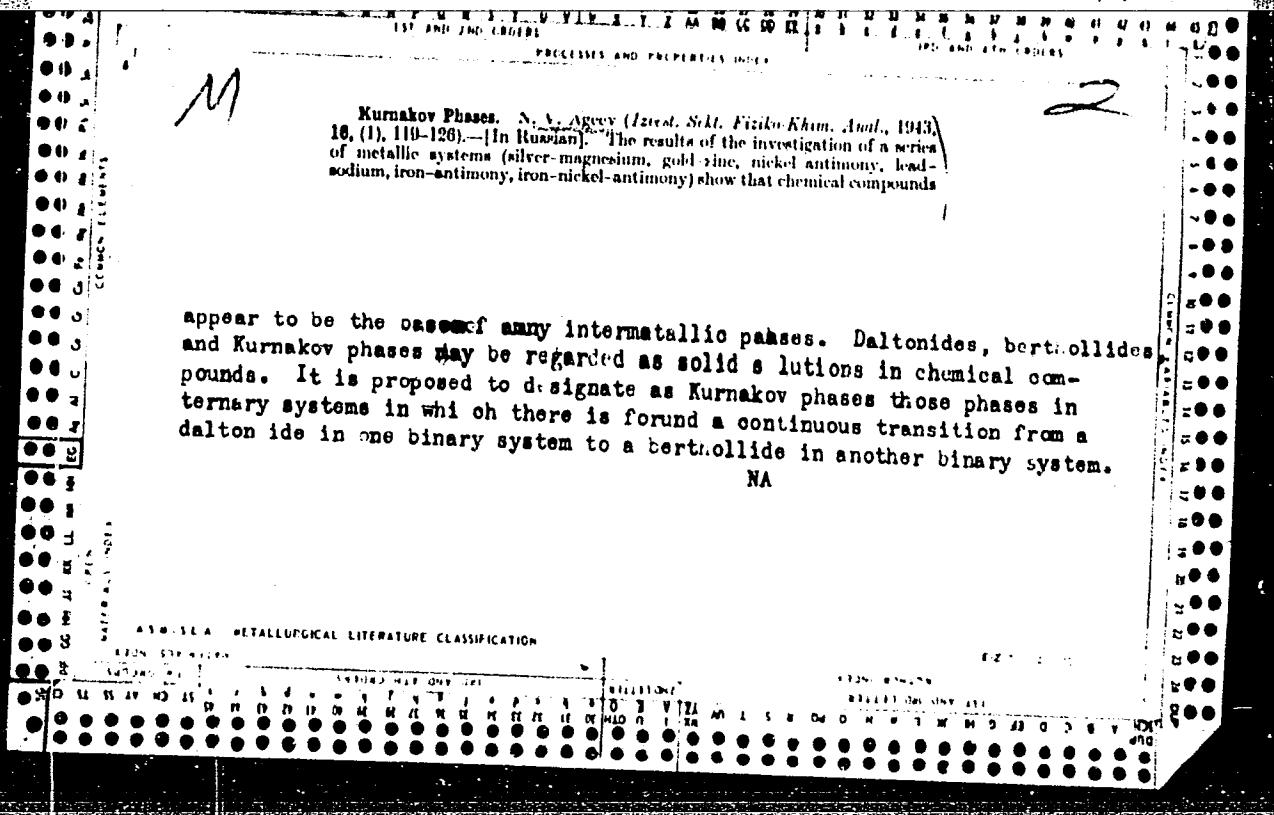
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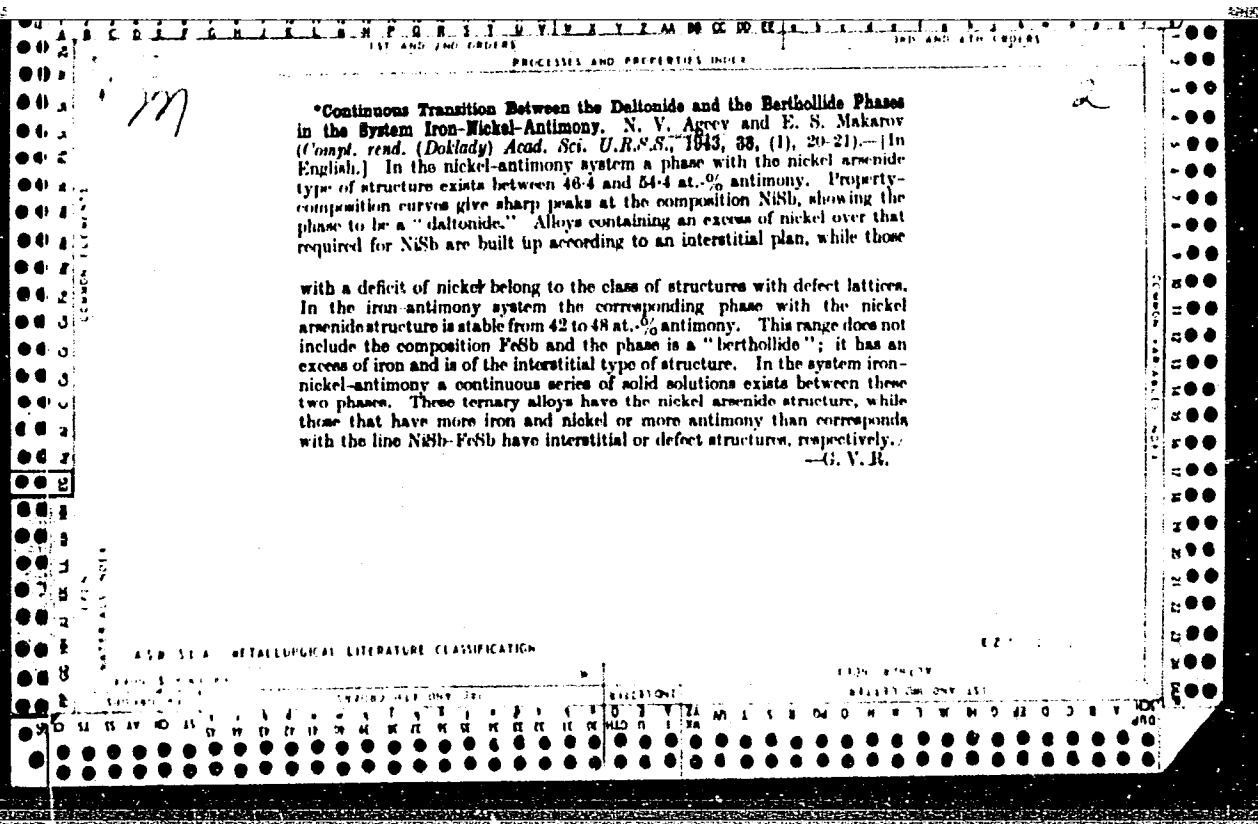
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AGEYEV, N. V.

"Continuous transition between the daltonide and the berthollide phases in the system Fe-Ni-Sb." The alloys were prepared from electrolytic Fe, Ni and Sb, homogenized at 600° for 3 days, slowly cooled at room temperature and then studied. These studies show the formation of a continuous series of solid solns. between 2 isomorphous phases, one of which is daltonide (I) and the other a berthollide (II) (as is the case with the system investigated), is a very representative instance of a continuous transition from I to II and points to the common genetic nature of these compounds. (Published in the Compt. Rend., Acad. Sci., URSS, 38, 20-1, 1943 (in English)

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